

**THE SOUND OF A PULSATING SPHERE IN A RAREFIED GAS:  
CONTINUUM BREAKDOWN AT SHORT LENGTH- AND TIME-SCALES**

Y. Ben-Ami and A. Manela

Faculty of Aerospace Engineering, Technion - Israel Institute of Technology  
Haifa 32000 , Israel

February 2, 2019; revised April 2, 2019

---

Running title: The sound of a pulsating sphere in a rarefied gas  
37 pages and 9 figures  
Available in L<sup>A</sup>T<sub>E</sub>X 2<sub>ε</sub>

## Abstract

The pressure field of a pulsating sphere is a canonical problem in classical acoustics, used to illustrate the acoustic efficiency of a monopole source at continuum conditions. We consider the counterpart vibroacoustic and thermoacoustic problems in a rarefied gas, to investigate the effect of continuum breakdown on monopole radiation. Focusing on small-amplitude normal-to-boundary mechanical and heat-flux excitations, the perturbation field is analyzed in the entire range of gas rarefaction and input frequencies. Numerical calculations are carried out via the direct simulation Monte Carlo method, and are used to validate analytical predictions in the free-molecular and near-continuum regimes. In the latter, the regularized thirteen moments model (R13) is applied, to capture the system response at states where the Navier-Stokes-Fourier (NSF) description breaks down. Comparing with the continuum inviscid solution, the results quantitate the dampening effect of gas rarefaction on source point-wise strength and acoustic power. At near-continuum conditions, the acoustic field is composed of exponentially decaying “compression”, “thermal” and “Knudsen-layer” modes, reflecting thermoviscous and higher-order rarefaction effects. With reducing rarefaction, the contributions of the latter two modes vanish, and the former degenerates into the ideal-flow inverse-to-distance decaying wave. Stronger attenuation is obtained with increasing rarefaction, where boundary sphericity results in a “geometric reduction” of the molecular layer affected by the source. Notably, while the R13 model at low frequencies appears valid up to moderate gas rarefaction rates, both the NSF and R13 descriptions break down at common low Knudsen numbers at higher frequencies. Further study should therefore be carried out to extend the applicability of moment models to unsteady flows with short timescales.

# 1 Introduction

The pressure far field of an object executing small-amplitude motions in a quiescent fluid is a fundamental problem in acoustics, serving as a setup for examining the production and propagation of sound waves in a fluid. The problem has been studied extensively in the context of continuum mechanics and in various setups [1], characterizing the far-field radiation through the pressure point-wise amplitude and directivity fields. Simplified calculations have been initially presented for an ideal fluid [1], and extended later on to account for the attenuating impacts of fluid viscosity and heat conductivity [2]. In a parallel set of studies, the thermoacoustic sound generation by the unsteady heating of a stationary surface has been examined (see, e.g., Refs. [3–5], and works cited therein). This type of acoustic excitation has been applied to develop the *thermophone* [6–8] as a means for sound generation with no moving parts.

A key outcome of the above investigations has been the determination of the acoustic waves speed and decay rate. While these have shown to agree well with measurements at low and intermediate frequencies, significant discrepancies have appeared at high frequencies [9–11]. These revealed the inadequacy of the continuum description to account for the phase speed and attenuation rate at non-continuum conditions, invoking the study of rarefaction effects on sound wave propagation.

The propagation of sound waves in rarefied gases has been investigated in a considerable number of works. These become relevant wherever the characteristic lengthscale, or timescale, of the setup involved are of the order of the molecular mean free path, or time, respectively. In vibroacoustic applications, such scenarios are common in micromechanical oscillators, where short length scales and high frequencies occur [12–14]. Focusing on a planar vibrating surface (see Refs. [15–18] and papers cited therein), existing studies have analyzed the attenuating effect of gas rarefaction, resulting in decay rates larger than at continuum conditions. Considering a stationary plane, counterpart studies have examined the perturbation field generated by time temperature variations of the boundary [19–23]. Later works have demonstrated that thermoacoustic sound, caused by boundary heat-flux excitations, may be applied for monitoring the sound of a vibrating planar object [24, 25].

In difference from the above planar-setup investigations, sound wave generation by non-planar objects at rarefied flow conditions has been studied in only few works. These include the acoustic field analyses of a pulsating cylindrical source carried out by Kalempa and Sharipov [26] and Ben-Ami and Manela [27], as well as the hydrodynamic perturbations induced by small-amplitude translations of a rigid sphere, considered by Yap and Sader [28]. Retaining a fixed volume, the sphere translations in Ref. [28] were used to model a *dipole* source, which is of weaker strength than its counterpart volume-varying *monopole* [1]. It is therefore of interest to complement these studies and consider the vibro- and thermo-acoustic efficiencies of a three-dimensional monopole at non-continuum conditions.

While acknowledging the fundamental interest in studying the canonical pulsating-sphere setup, the results of such a study may also be of practical value for the analysis of the acoustic field of vibrating nanoscale particles, where both shape and volume variations take form [29, 30]. In this context, the past decade has evidenced growing interest in the investigation of small-scale micro and nanoparticle vibrations (see Crut *et al.* [31], and an abundance of references cited therein). Due to the small size of the particles, quantitative assessment of their internal structural, morphological and mechanical properties require the application of non-conventional (indirect) measurement techniques. The method of time-resolved spectroscopy is often used for this purpose. The method applies pulsed-laser signals to trigger acoustic oscillations within the particles, through which their properties of interest are captured. The particles response, characterized by their oscillation frequencies and dampening time-scales, depends strongly on their interaction with the surrounding medium [29, 32]. It is therefore of evident importance to study the coupled gas response to acoustic vibrations at small scales, where traditional continuum models break down.

The dynamics of rarefied gas flows are governed by the Boltzmann equation, valid at length- and times-scales that are larger than the molecular diameter and collision duration, respectively. However, due to the complexity of the kinetic equation, analytical treatments are traditionally limited to the regimes of high (ballistic) and low (continuum-limit) Knudsen (Kn) numbers, whereas the intermediate domain of  $\text{Kn} \sim O(1)$  is studied numerically via direct finite-difference-based solutions of the equation or molecular simulations. Notably, the characteristically small

excitation amplitudes involved in acoustic problems make the latter approach computationally expensive, and the advantage of obtaining analytical approximations is apparent.

Recent years have shown significant progress in the study of moment equations and their application for the modeling of rarefied gas flows at low and intermediate Knudsen numbers. Originally introduced by Grad [33], these methods obtain closed-form sets of hydrodynamic-type equations from the Boltzmann equation, in an effort to capture non-small rarefaction effects. Recent progress has been initiated by Struchtrup and Torrilhon (see Refs. [34, 35] and papers cited therein), who formulated the regularized set of thirteen moment equations (R13). Gu and Emerson [36] have complemented the model by deriving the boundary conditions to be imposed at a solid diffuse or specular reflecting surface for Maxwell-type molecules. These conditions have been reassessed by Torrilhon and Struchtrup [37], who overcame some inconsistencies prevailing at non-linear flow conditions. The R13 and higher order models have been later on applied to investigate a series of steady rarefied gas flows, recently reviewed by Torrilhon [38]. Steady-state solutions for the R13 equations in spherical geometry were derived by Claydon *et al.* [39].

In light of the above, the objective of the present contribution is to analyze the effect of gas rarefaction on the acoustic field of a mechanically actuated (through boundary pulsations) and thermally excited (via normal heat-flux) solid sphere. The sphere radius and excitation timescale are chosen so that non-continuum flow conditions prevail, and the problem is investigated in the entire range of gas rarefaction rates. Analytical investigations are carried out in the limits of low (continuum and early transition) and high (free-molecular) Knudsen numbers, and are accompanied by direct simulation Monte-Carlo (DSMC) calculations. An analytical solution is derived using the R13 equations, which is found valid at non-small Knudsen numbers (up to  $\text{Kn} \approx 0.6$ ) for low enough excitation frequencies. The R13 predictions reveal the appearance of a high-order Knudsen-layer mode, which is missing from the Navier-Stokes description.

In the next section, the pulsating sphere problem is formulated. The analytical treatments in the near-continuum and free-molecular limits are described in Secs. 3 and 4, respectively, followed by an outline of the numerical DSMC scheme in Sec. 5. Our results are presented in Sec. 6, where the domains of applicability of the limit-case analyses are delineated, and the acoustic fields of a

pulsating adiabatic sphere and a stationary heated surface are described. Concluding remarks are given in Sec. 7.

## 2 Statement of the problem

Consider a semi-confined monoatomic gas layer of uniform density  $\rho_0^*$  and temperature  $T_0^*$  surrounding an impermeable sphere of radius  $r^* = r_0^*$  (hereafter asterisks denote dimensional quantities). The gas is initially at rest and in thermodynamic equilibrium with the sphere. At time  $t^* \geq 0$ , radial surface pulsations are imposed with velocity

$$\varepsilon \mathbf{U}_w^*(t^*) = \varepsilon U_w^*(t^*) \hat{\mathbf{r}}, \quad (1)$$

together with normal heat-flux excitations

$$\varepsilon \mathbf{Q}_w^*(t^*) = \varepsilon Q_w^*(t^*) \hat{\mathbf{r}}. \quad (2)$$

In Eqs. (1) and (2),  $\hat{\mathbf{r}}$  marks a unit vector in the radial direction, and  $\varepsilon \ll 1$ , so that the system description may be linearized about its initial equilibrium. In practice, the monitoring of time-varying heat-flux excitations requires the determination of the amount of energy that is transmitted to the gas. A similar issue, concerning the evaluation of energy transmission efficiency, has been considered in the context of the thermophone device (see Refs. [8, 40], and works cited therein). Accordingly, a more comprehensive formulation would couple the thermoacoustic gas state to a heat-conduction problem within the sphere. This calculation would involve the replacement of the boundary condition (2) with appropriate matching conditions of heat-fluxes and temperatures between the solid and fluid sides of the sphere. The solution of the coupled problem should yield a transfer function relating the amount of invested energy and the heat-flux transmitted to the gas, affected by the thermal properties of the solid material. Such analysis is not followed in the present work, which focuses on the effect of gas rarefaction on monopole sound radiation. In particular, a large portion of our discussion focuses on the generation of sound by an adiabatic (thermally insulating) sphere, which may be easily realized in experiments.

In what follows we analyze the gas response to sphere actuations in the entire range of sphere radii and excitation time scales relative to their counterpart molecular quantities. While the analysis is carried out in part for *arbitrary* small-amplitude actuations (see Sec. 4), our results are presented for harmonic wall excitations,

$$U_w^*(t^*) = \overline{U}_w^* \cos(\omega^* t^*) \quad \text{and} \quad Q_w^*(t^*) = \overline{Q}_w^* \cos(\omega^* t^*), \quad (3)$$

where  $\omega^*$  denotes the common mechanical and heat-flux actuation frequency, and we focus on the final time-periodic state of the system. Here,  $\varepsilon$  has been omitted for convenience, yet the numerical values of  $\overline{U}_w^*$  and  $\overline{Q}_w^*$  will be taken small in their normalized form.

Further analysis requires the scaling of the problem. To this end we normalize the length and velocity by the nominal sphere radius  $r_0^*$  and molecular mean thermal speed  $U_{\text{th}}^* = \sqrt{2\mathcal{R}^* T_0^*}$  (where  $\mathcal{R}^*$  marks the specific gas constant), respectively. The non-dimensional problem is then governed by the gas mean Knudsen number and scaled frequency,

$$\text{Kn} = l_0^*/r_0^* \quad \text{and} \quad \omega = \omega^* r_0^*/U_{\text{th}}^*, \quad (4)$$

respectively, where  $l_0^*$  marks the molecular mean free path, specified after Eq. (17). In terms of the governing parameters, it is expected that free molecular conditions should prevail when  $\text{Kn} \gg 1$  or  $\omega \text{Kn} \gg 1$ , for which either the lengthscale or timescale are short compared with the mean free path or mean free time, respectively. In contrast, as will be discussed in Sec. 6, continuum-limit conditions require that both  $\text{Kn} \ll 1$  and  $\omega^2 \text{Kn} \ll 1$ . For later convenience we denote

$$\text{Kn}_\omega = \omega \text{Kn} = \omega^* l_0^*/U_{\text{th}}^*, \quad (5)$$

as the frequency-based Knudsen number, representing the ratio between the excitation frequency and the molecular collision frequency. Following analysis will be presented in terms of  $\text{Kn}$  and  $\omega$ , while  $\text{Kn}_\omega$  will be used to facilitate the discussion in Sec. 6.

To better assess the effect of gas rarefaction on the acoustic efficiency of the source, we recapitulate the known result for the acoustic field of a pulsating sphere at continuum inviscid ( $\text{Kn}, \omega \text{Kn} \rightarrow 0$ ) conditions [1]. Considering the case of harmonic mechanical actuations only

( $\overline{U}_w \neq 0, \overline{Q}_w = 0$ ), the far-field acoustic pressure and radial velocity are given by

$$\begin{aligned} p_{\text{inviscid}}(r, t) &= \frac{\overline{U}_w \omega}{r(1 + \omega^2/c_0^2)} \left[ \frac{\omega}{c_0} \cos(\omega t_r) - \sin(\omega t_r) \right] \quad \text{and} \\ u_{\text{inviscid}}(r, t) &= \frac{\overline{U}_w \omega}{rc_0(1 + \omega^2/c_0^2)} \left[ \frac{\omega}{c_0} \left( \frac{c_0^2}{\omega^2 r} + 1 \right) \cos(\omega t_r) + \left( \frac{1}{r} - 1 \right) \sin(\omega t_r) \right], \end{aligned} \quad (6)$$

respectively, where  $t_r = t - (r - 1)/c_0$  is the acoustic retarded time (with  $r$  denoting the scaled radial distance from the sphere center), and  $c_0$  marks the mean speed of sound scaled by the mean thermal speed,  $c_0^*/U_{th}^*$ . For an ideal monatomic gas considered hereafter,  $c_0^* = \sqrt{\gamma \mathcal{R}^* T_0^*}$  (where  $\gamma = 5/3$  marks the ratio of gas specific heats), and  $c_0 = \sqrt{5/6}$ . The overall source strength is evaluated through its acoustic power

$$\Pi(r, t) \equiv \oint_{\tilde{r}=r} p(\tilde{r}, t) u(\tilde{r}, t) dS, \quad (7)$$

where the integration is carried out over a spherical surface  $S$  of radius  $\tilde{r} > 1$  centered at  $\tilde{r} = 0$ . To obtain a time-independent result, we define the time-averaged acoustic power,

$$\bar{\Pi}(r) = \frac{1}{T} \int_0^T \Pi(r, t) dt, \quad (8)$$

obtained by integrating  $\Pi(r, t)$  over a period  $T = 2\pi/\omega$ . Substituting Eq. (6) into Eq. (7) and then into (8), we obtain for the inviscid far-field limit

$$\bar{\Pi}_{\text{inviscid}}(r \gg 1) \approx 2\pi \overline{U}_w^2 \sqrt{\frac{6}{5}} \left( \frac{\omega^2}{1 + 6\omega^2/5} \right). \quad (9)$$

The result is independent of  $r \gg 1$  due to the  $r^{-1}$  leading order decay of  $p_{\text{inviscid}}$  and  $u_{\text{inviscid}}$ , and thus remains unchanged at arbitrarily large distances from the source. As will be shown in Secs. 3 and 4, non-zero gas rarefaction results in stronger decay rates which, in turn, lead to a decrease in (and far-field vanishing of) the acoustic power with increasing  $r$  (see Fig. 7).

### 3 Near-continuum conditions

To analyze the problem at relatively small Knudsen numbers, we make use of the hydrodynamic R13 model mentioned in the Introduction [34, 35]. The scheme has been derived for a Maxwell-type model of molecular interaction, where the three-dimensional formulation consists of balances



for the scalar density and pressure, the vectors of velocity and heat-flux, and the stress tensor. Higher order moments are coupled to the system through a Chapman-Enskog-type expansion of the probability density function in the kinetic Boltzmann equation. In this work, we apply the R13 model for an unsteady, one-dimensional ( $r$ -dependent) and linearized setup. Focusing on the case of sinusoidal excitation specified in Eq. (3), we assume harmonic time dependence of all hydrodynamic perturbations,

$$\Phi(r, t) = \text{Re} \left\{ \bar{\Phi}(r) \exp[i\omega t] \right\}. \quad (10)$$

Using spherical coordinates, the macroscopic balances of continuity,  $r$ -momentum, and energy are given by

$$i\omega\bar{\rho} + \frac{1}{r^2} \frac{d}{dr} (r^2 \bar{u}) = 0, \quad (11)$$

$$i\omega\bar{u} = -\frac{d\bar{p}}{dr} - \frac{1}{r^3} \frac{d}{dr} (r^3 \bar{\sigma}), \quad (12)$$

and

$$i\omega\bar{T} = -\frac{2}{3r^2} \frac{d}{dr} [r^2 (\bar{u} + 2\bar{q})], \quad (13)$$

respectively, and are supplemented by the linearized form of the equation of state,

$$\bar{p} = (\bar{\rho} + \bar{T})/2. \quad (14)$$

Appearing in Eqs. (11)-(14) are the amplitudes of the density perturbation  $\bar{\rho}(r)$ , radial velocity  $\bar{u}(r)$ , pressure  $\bar{p}(r)$ , and temperature  $\bar{T}(r)$ . Also appearing in Eqs. (12)-(13) are the amplitudes of the radial normal stress  $\bar{\sigma}(r)$ , and the radial heat-flux  $\bar{q}(r)$ , which satisfy the additional equations

$$i\omega\bar{\sigma} + \frac{1}{r^4} \frac{d}{dr} (r^4 \bar{m}) = -\frac{\bar{\sigma}}{2\text{Kn}} - \frac{2r}{3} \frac{d}{dr} \left[ r^{-1} \left( \bar{u} + \frac{4}{5} \bar{q} \right) \right] \quad (15)$$

and

$$i\omega\bar{q} + \frac{1}{2r^3} \frac{d}{dr} (r^3 \bar{R}) = -\frac{\bar{q}}{3\text{Kn}} - \frac{1}{2r^3} \frac{d}{dr} (r^3 \bar{\sigma}) - \frac{5}{8} \frac{d\bar{T}}{dr} - \frac{1}{6} \frac{d\bar{\Delta}}{dr}. \quad (16)$$

Equations (15) and (16) couple the higher-order moments' amplitude functions  $\bar{m}(r)$ ,  $\bar{R}(r)$  and  $\bar{\Delta}(r)$ , which are fixed through a linearized form of the closure relations derived by Struchtrup and Torrilhon [34],

$$\bar{m} = -\frac{6\text{Kn}}{5} r^2 \frac{d}{dr} (r^{-2} \bar{\sigma}) \quad , \quad \bar{R} = -\frac{16\text{Kn}}{5} r \frac{d}{dr} (r^{-1} \bar{q}) \quad \text{and} \quad \bar{\Delta} = -\frac{12\text{Kn}}{r^2} \frac{d}{dr} (r^2 \bar{q}). \quad (17)$$

The Knudsen number appearing in Eqs. (15)-(17) is given by

$$\text{Kn} = \nu_0^*/r_0^*U_{\text{th}}^*,$$

where  $l_0^* = \nu_0^*/U_{\text{th}}^*$  in accordance with Eq. (4). At continuum-limit conditions,  $\nu_0^*$  marks the coefficient of kinematic viscosity. Equations (11)-(17) are supplemented by the conditions of impermeability and normal heat flux at the sphere surface (see Eqs. (1)-(2)),

$$\bar{u}(1) = \bar{U}_w \quad \text{and} \quad \bar{q}(1) = \bar{Q}_w, \quad (18)$$

together with a high-order moment condition obtained from Gu and Emerson [36],

$$-\frac{6}{\sqrt{\pi}}\bar{\sigma}(1) - \frac{6}{7\sqrt{\pi}}\bar{R}(1) - 4\bar{m}(1) = \bar{U}_w + \frac{4}{5}\bar{Q}_w, \quad (19)$$

and far-field decay conditions. As expected, a temperature jump condition is missing from the present formulation, and replaced by the heat-flux condition in Eq. (18). The condition (19) is derived by eliminating the unknown wall temperature from the linearized version of conditions (30) and (31) in Gu and Emerson [36] (or, alternatively, Eqs. (35) and (36) in Torrilhon and Struchtrup [37]). Note that in both Refs. [36] and [37], the boundary considered is not shifted in the normal direction, in difference from the present setup. Hence, the wall normal velocity contribution should be added, similarly to Rana *et al.* [41] and Beckman *et al.* [42], in the context of evaporation-driven flows.

The system of equations may be recast to form a single triharmonic equation for  $\bar{T}(r)$ ,

$$\begin{aligned} & \text{Kn}^3 \left[ 1 + \frac{36}{5}i\omega\text{Kn} \right] \nabla_r^6 \bar{T} - \frac{5}{12}\text{Kn} \left[ 1 + \frac{62}{5}i\omega\text{Kn} - \frac{888}{25}(\omega\text{Kn})^2 - \frac{2592}{125}i(\omega\text{Kn})^3 \right] \nabla_r^4 \bar{T} \\ & + \frac{5}{18}i\omega \left[ 1 + \frac{48}{5}i\omega\text{Kn} - \frac{864}{25}(\omega\text{Kn})^2 - \frac{864}{25}i(\omega\text{Kn})^3 \right] \nabla_r^2 \bar{T} + \frac{1}{3}i\omega^3 \left[ 1 + 5i\omega\text{Kn} - 6(\omega\text{Kn})^2 \right] \bar{T} = 0, \end{aligned} \quad (20)$$

where  $\nabla_r^2 = r^{-2} \frac{d}{dr} \left( r^2 \frac{d}{dr} \right)$  denotes the  $r$ -dependent part of the Laplace operator. The equation is subject to the solution

$$\bar{T}(r) = \sum_{n=1}^6 \alpha_n \Theta_n(r), \quad (21)$$

where  $\alpha_n$  are constants and  $\Theta_n(r)$  satisfy the Helmholtz equation

$$\nabla_r^2 \Theta_n = \lambda_n^2 \Theta_n. \quad (22)$$

In Eq. (22),  $\lambda_n$  are the roots of the characteristic polynomial of Eq. (20). Expanding in  $\text{Kn} \ll 1$ , the leading-order expressions for  $\lambda_n$  are

$$\lambda_{1\pm} \approx \pm \sqrt{\frac{6}{5}} \left( \frac{7}{5} \omega^2 \text{Kn} + i\omega \right), \quad \lambda_{2\pm} \approx \pm \sqrt{\frac{1}{3} \frac{\omega}{\text{Kn}}} (1 + i) \quad \text{and} \quad \lambda_{3\pm} \approx \pm \sqrt{15} \left( \frac{1}{6} \text{Kn}^{-1} + \frac{3}{10} i\omega \right), \quad (23)$$

and the general solution for  $\bar{T}(r)$  may be put in the form

$$\bar{T}(r) = \sum_{n=1}^3 \left\{ a_n \frac{\sin(i\lambda_n r)}{i\lambda_n r} + b_n \frac{\cos(i\lambda_n r)}{i\lambda_n r} \right\}. \quad (24)$$

Expecting a casual outward radiating signal, we set  $a_n = ib_n$ , which ensures that no incoming propagating wave is contained, to yield

$$\bar{T}(r) = \sum_{n=1}^3 C_n \frac{\exp[-\lambda_n r]}{r}. \quad (25)$$

For later reference, we denote the  $\lambda_1, \lambda_2$  and  $\lambda_3$  components of the solution by “compression”, “thermal” and “Knudsen layer” modes, respectively. The compression mode is characterized by the slowest decay rate at low  $\text{Kn}$ , and therefore dominates the far field response, whereas the thermal and Knudsen layer components decay much stronger. In particular, the Knudsen layer mode decays at rate  $\sim \exp[-\sqrt{15}\text{Kn}^{-1}r/6]$ , and is therefore significant only in an  $O(\text{Kn})$  (Knudsen layer) vicinity of the wall. Yet, apart from its direct effect on the gas behavior inside the layer, it affects the values of the constants  $C_1$  and  $C_2$  multiplying the  $\lambda_{1,2}$  modes, which then modify the gas behavior in the entire domain. For later discussion we note that the leading-order decay rate of  $\lambda_3$  is independent of the excitation frequency, and is therefore not affected by a change in the system timescale.

Having solved for  $\bar{T}(r)$ , expressions for all other hydrodynamic fields follow by substitutions of Eq. (25) into the above set of balance equations, as specified in Appendix A. Importantly, all fields combine the three decaying components contained in Eq. (25). The constants  $C_n$  are fixed using the conditions in Eqs. (18) and (19).

### 3.1 The Navier-Stokes-Fourier limit

To assess the differences between the R13 and continuum-limit solutions, it is instructive to derive the Navier-Stokes-Fourier (NSF) description of the system. Either by replacing Eqs. (15) and

(16) with the Newtonian and Fourier constitutive relations for  $\bar{\sigma}(r)$  and  $\bar{q}(r)$ , respectively, or by taking the consistent  $Kn \ll 1$  leading order limit of Eq. (20), the problem for  $\bar{T}(r)$  reduces to the biharmonic equation

$$\frac{5}{4}Kn\nabla_r^4\bar{T} + \frac{\omega}{6}(-5i + 23\omega Kn)\nabla_r^2\bar{T} - i\omega^3\bar{T} = 0. \quad (26)$$

In difference from the R13 result, the reduction in the equation order leads to the solution

$$\bar{T}(r) = \sum_{n=1}^2 D_n \frac{\exp[-\lambda_n^{\text{NSF}} r]}{r}, \quad (27)$$

where

$$\lambda_{1\pm}^{\text{NSF}} \approx \pm \sqrt{\frac{6}{5}} \left( \frac{7}{5} \omega^2 Kn + i\omega \right) \quad \text{and} \quad \lambda_{2\pm}^{\text{NSF}} \approx \pm \sqrt{\frac{1}{3} \frac{\omega}{Kn}} (1 + i) \quad (28)$$

are the roots of the characteristic polynomial corresponding to Eq. (26).

Inspecting the similarities between the NSF and R13 results, we observe that the leading orders of  $\lambda_{1,2}$  in Eq. (23) and  $\lambda_{1,2}^{\text{NSF}}$  in Eq. (28) are identical. The higher order corrections, not specified here for brevity, differ in some quantitative details. Yet more importantly, the reduction in problem order in the NSF model results in the omission of the  $\lambda_3$  mode from the NSF description. At small enough  $Kn$ , these differences have only a minor effect on the results, as the Knudsen layer (and its associated outer-layer impact) diminishes. At non-vanishing  $Kn$ , however, the effect of the Knudsen layer becomes significant, contributing to the breakdown of the NSF description. As demonstrated by the results in Sec. 6, the R13 model remains valid in part of these parameter combinations, yielding predictions that are in agreement with DSMC computations.

## 4 Free-molecular limit

Free molecular conditions should prevail wherever  $Kn \gg 1$  or  $Kn_\omega = \omega Kn \gg 1$ , for which either the lengthscale or timescale are short compared with the mean free path or mean free time, respectively. For the spherically-symmetric setup considered, the gas state is governed by the probability density function  $f = f(r, t, \xi)$  of finding a gas molecule with velocity and radial

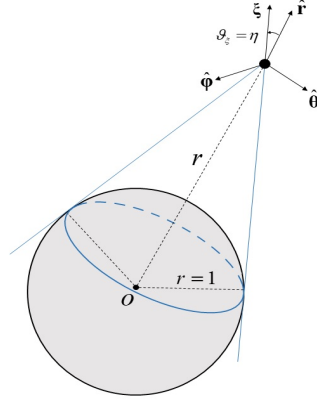


Figure 1: Schematic of the system parametrization in the free-molecular limit. The bold point marks the position of an arbitrary particle, and the outer-sphere volume confined by the blue lines and the spherical cap denotes the  $\vartheta_\xi$ -interval acquired by the particle when reflected from the spherical surface.

position about  $\xi$  and  $r$ , respectively, at time  $t$ . Expanding  $f(r, t, \xi)$  about its initial non-dimensional Maxwellian distribution  $F = \pi^{-3/2} \exp[-\xi^2]$ , we write

$$f(r, t, \xi) = F [1 + h(r, t, \xi)], \quad (29)$$

where  $h(r, t, \xi)$  denotes the unknown small ( $|h| \ll 1$ ) perturbation function due to sphere excitations. At free-molecular conditions,  $h(r, t, \xi)$  satisfies the collisionless one-dimensional ( $r$ -dependent) Boltzmann equation in spherical coordinates  $(r, \theta, \varphi)$  [43],

$$\frac{\partial h}{\partial t} + \xi_r \frac{\partial h}{\partial r} + \frac{\xi_\theta^2 + \xi_\varphi^2}{r} \frac{\partial h}{\partial \xi_r} + \frac{1}{r} \left( \frac{\xi_\varphi^2}{\tan \theta} - \xi_r \xi_\theta \right) \frac{\partial h}{\partial \xi_\varphi} - \frac{\xi_\varphi}{r} \left( \frac{\xi_\theta}{\tan \theta} + \xi_r \right) \frac{\partial h}{\partial \xi_\varphi} = 0, \quad (30)$$

where the system parametrization is specified in Fig. 1. Performing the variable transformation

$$\xi = \sqrt{\xi_r^2 + \xi_\theta^2 + \xi_\varphi^2}, \quad \cos \vartheta_\xi = \frac{\xi_r}{\xi} \quad \text{and} \quad \tan \phi_\xi = \frac{\xi_\theta}{\xi_\varphi}, \quad (31)$$

Eq. (30) assumes the form

$$\frac{\partial h}{\partial t} + \xi \cos \vartheta_\xi \frac{\partial h}{\partial r} - \frac{\xi \sin \vartheta_\xi}{r} \frac{\partial h}{\partial \vartheta_\xi} + \tan \theta \frac{\xi \sin \vartheta_\xi \cos \phi_\xi}{r} \frac{\partial h}{\partial \phi_\xi} = 0. \quad (32)$$

The equation is supplemented by the initial condition

$$h(r, t = 0^-, \xi, \vartheta_\xi, \phi_\xi) = 0, \quad (33)$$

together with a linearized form of the diffuse boundary condition at the spherical surface,

$$h(r = 1, 0 \leq \vartheta_\xi \leq \pi/2) = \rho_w(t) + 2\xi \cos \vartheta_\xi U_w(t) + (\xi^2 - 3/2) T_w(t), \quad (34)$$

applied to the reflected  $\xi_r > 0$  molecules at  $r = 1$ . Here,  $\rho_w(t)$  and  $T_w(t)$  are treated unknown, with the latter denoting the time perturbation of the sphere temperature about  $T_0 = 1$ .

Inspecting Eq. (34), it is noted that the boundary condition is independent of  $\phi_\xi$ . Since boundary excitation is the only cause for system deviation from equilibrium in the present problem, we assume that  $h \neq h(\phi_\xi)$ , and Eq. (32) reduces to

$$\frac{\partial h}{\partial t} + \xi \cos \vartheta_\xi \frac{\partial h}{\partial r} - \frac{\xi \sin \vartheta_\xi}{r} \frac{\partial h}{\partial \vartheta_\xi} = 0. \quad (35)$$

Eq. (35) is amenable to the closed-form solution

$$h(r, t, \xi, \vartheta_\xi, \phi_\xi) = \begin{cases} \rho_w(t_w) + 2\xi U_w(t_w) \sqrt{1 - r^2 \sin^2 \vartheta_\xi} + T_w(t_w) (\xi^2 - 3/2), & \vartheta_\xi \leq \eta \\ 0 & \eta < \vartheta_\xi \leq \pi, \end{cases} \quad (36)$$

where

$$t_w = t - \left( r \cos \vartheta_\xi - \sqrt{1 - r^2 \sin^2 \vartheta_\xi} \right) / \xi \equiv t - x_w(r, \vartheta_\xi) / \xi$$

is the molecular-level retarded time in the ballistic limit. In addition,

$$\eta = \sin^{-1}(1/r),$$

also indicated in Fig. 1.

To determine  $\rho_w(t)$  and  $T_w(t)$ , the macroscopic conditions of impermeability,

$$\frac{1}{\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^\infty h(r = 1) \xi^3 \sin 2\vartheta_\xi \exp[-\xi^2] d\xi = U_w(t), \quad (37)$$

and heat-flux,

$$\frac{1}{2\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^\infty h(r = 1) \xi^5 \sin 2\vartheta_\xi \exp[-\xi^2] d\xi - \frac{5}{4} U_w(t) = Q_w(t), \quad (38)$$

are imposed at the walls, yielding

$$\rho_w(t) = \frac{7\sqrt{\pi}}{8} U_w(t) - \sqrt{\pi} Q_w(t) \quad \text{and} \quad T_w(t) = \frac{\sqrt{\pi}}{4} U_w(t) + 2\sqrt{\pi} Q_w(t). \quad (39)$$

Substituting Eq. (39) into (36) and then into (29), the density, radial velocity, pressure, and radial heat-flux perturbations may be computed via velocity-space quadratures over the probability density function. Specifically,

$$\begin{aligned}
\rho(r, t) &= \frac{2}{\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^\infty h(r, t, \xi, \vartheta_\xi) \xi^2 \sin \vartheta_\xi \exp[-\xi^2] d\xi, \\
u(r, t) &= \frac{1}{\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^\infty h(r, t, \xi, \vartheta_\xi) \xi^3 \sin 2\vartheta_\xi \exp[-\xi^2] d\xi, \\
p(r, t) &= \frac{2}{3\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^\infty h(r, t, \xi, \vartheta_\xi) \xi^4 \sin \vartheta_\xi \exp[-\xi^2] d\xi \quad \text{and} \\
q(r, t) &= \frac{1}{2\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^\infty h(r, t, \xi, \vartheta_\xi) \xi^5 \sin 2\vartheta_\xi \exp[-\xi^2] d\xi - \frac{5}{4} u(r, t),
\end{aligned} \tag{40}$$

whereas the temperature perturbation is given by the linearized form of the equation of state,

$$T(r, t) = 2p(r, t) - \rho(r, t). \tag{41}$$

Evaluation of the integrals in Eq. (40) is facilitated by carrying a change in variables

$\tau = t - x_w(r, \vartheta_\xi)/\xi$ , to yield

$$\begin{aligned}
\rho(r, t) &= \frac{2}{\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^t \hat{h}(r, t, \tau, \vartheta_\xi) \frac{x_w^3}{(t-\tau)^4} \sin \vartheta_\xi \exp\left[-\left(\frac{x_w}{t-\tau}\right)^2\right] d\tau, \\
u(r, t) &= \frac{1}{\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^t \hat{h}(r, t, \tau, \vartheta_\xi) \frac{x_w^4}{(t-\tau)^5} \sin 2\vartheta_\xi \exp\left[-\left(\frac{x_w}{t-\tau}\right)^2\right] d\tau, \\
p(r, t) &= \frac{2}{3\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^t \hat{h}(r, t, \tau, \vartheta_\xi) \frac{x_w^5}{(t-\tau)^6} \sin \vartheta_\xi \exp\left[-\left(\frac{x_w}{t-\tau}\right)^2\right] d\tau \quad \text{and} \\
q(r, t) &= \frac{1}{2\sqrt{\pi}} \int_0^\pi d\vartheta_\xi \int_0^t \hat{h}(r, t, \tau, \vartheta_\xi) \frac{x_w^6}{(t-\tau)^7} \sin 2\vartheta_\xi \exp\left[-\left(\frac{x_w}{t-\tau}\right)^2\right] d\tau - \frac{5}{4} u(r, t),
\end{aligned} \tag{42}$$

where

$$\hat{h}(r, t, \tau, \vartheta_\xi) = \begin{cases} \rho_w(\tau) - \frac{3}{2} T_w(\tau) + \frac{2x_w}{t-\tau} U_w(\tau) \sqrt{1 - r^2 \sin^2 \vartheta_\xi} + \left(\frac{x_w}{t-\tau}\right)^2 T_w(\tau), & \vartheta_\xi \leq \eta \\ 0 & \eta < \vartheta_\xi \leq \pi. \end{cases}$$

The hydrodynamic fields can now be calculated via numerical integration. Towards this end, introduce

$$\begin{aligned}
I_n^{(m)} &= \frac{1}{\sqrt{\pi}} \int_0^\eta d\vartheta_\xi \int_0^\infty U_w(t_w) \sqrt{1 - r^2 \sin^2 \vartheta_\xi} f^{(m)}(\vartheta_\xi) \xi^n \exp[-\xi^2] d\xi, \\
J_n^{(m)} &= \frac{1}{\sqrt{\pi}} \int_0^\eta d\vartheta_\xi \int_0^\infty \rho_w(t_w) f^{(m)}(\vartheta_\xi) \xi^n \exp[-\xi^2] d\xi \quad \text{and} \\
K_n^{(m)} &= \frac{1}{\sqrt{\pi}} \int_0^\eta d\vartheta_\xi \int_0^\infty T_w(t_w) f^{(m)}(\vartheta_\xi) \exp[-\xi^2] d\xi,
\end{aligned} \tag{43}$$

with  $m = 1, 2$  and

$$f^{(m)} = \begin{cases} \sin \vartheta_\xi, & m = 1 \\ \sin 2\vartheta_\xi, & m = 2, \end{cases}$$

to cast Eq. (42) in the form

$$\begin{aligned} \rho(r, t) &= 4I_3^{(1)} + 2J_2^{(1)} - 3K_2^{(1)} + 2K_4^{(1)}, \\ u(r, t) &= 2I_4^{(2)} + J_3^{(2)} - \frac{3}{2}K_3^{(2)} + K_5^{(2)}, \\ p(r, t) &= \frac{1}{3} \left( 4I_5^{(1)} + 2J_4^{(1)} - 3K_4^{(1)} + 2K_6^{(1)} \right), \\ T(r, t) &= \frac{1}{3} \left( -12I_3^{(1)} + 8I_5^{(1)} - 6J_2^{(1)} + 4J_4^{(1)} + 9K_2^{(1)} - 9K_4^{(1)} + 4K_6^{(1)} \right) \quad \text{and} \\ q(r, t) &= \frac{1}{8} \left( -20I_4^{(2)} + 8I_6^{(2)} - 10J_3^{(2)} + 4J_5^{(2)} + 15K_3^{(2)} - 16K_5^{(2)} + 4K_7^{(2)} \right). \end{aligned} \quad (44)$$

In difference from analysis in Sec. 3, the solution in the free-molecular regime, involving the numerical evaluation of  $I_n^{(m)}$ ,  $J_n^{(m)}$  and  $K_n^{(m)}$ , is valid for *arbitrary* small-amplitude  $U_w(t)$  and  $Q_w(t)$  input signals. Focusing on the case of harmonic excitation specified in Eq. (3), explicit approximations for the hydrodynamic fields may be obtained for  $\omega(r-1) \gg 1$ . The approximation, presented in Appendix B, applies the method of steepest descent to evaluate the  $\xi$ -integrals, together with the method of stationary phase to estimate the  $\vartheta_\xi$ -integrals. These yield

$$\begin{aligned} I_n^{(1)} \approx J_n^{(1)} \approx K_n^{(1)} &\approx \text{Re} \left\{ \frac{1}{2r} \sqrt{\frac{z_0^{n-2}}{3^{n-1}}} \left[ 1 - e^{-\frac{z_0 r}{3} \eta^2} \right] \left( 1 + \frac{a_1}{z_0} + \frac{a_2}{z_0^2} \right) \exp[i\omega t - z_0] \right\} \\ \text{and } (I_n^{(2)}, J_n^{(2)}, K_n^{(2)}) &\approx 2(I_n^{(1)}, J_n^{(1)}, K_n^{(1)}), \end{aligned} \quad (45)$$

where  $z_0 = 3[\omega(r-1)/2]^{2/3} \exp[i\pi/3] \gg 1$ , and the expressions for the constants  $a_1$  and  $a_2$  are detailed in the Appendix. Substituting Eq. (45) into Eq. (44), we find that the decay rate of all hydrodynamic perturbations is

$$\mathcal{D} = \mathcal{D}_{\text{planar}} \mathcal{D}_{\text{curv}}, \quad (46)$$

where  $\mathcal{D}_{\text{planar}}$  marks the perturbations decay in the planar case [25],

$$\mathcal{D}_{\text{planar}} \approx \sqrt{\frac{z_0^{n-2}}{3^{n-1}}} \left( 1 + \frac{a_1}{z_0} + \frac{a_2}{z_0^2} \right) \exp[-z_0], \quad (47)$$



and  $\mathcal{D}_{curv}$  denotes the additional decay caused by source sphericity,

$$\mathcal{D}_{curv} \approx \frac{1}{2r} \left\{ 1 - \exp \left[ -\frac{z_0 r}{3} \left( \sin^{-1}(1/r) \right)^2 \right] \right\}. \quad (48)$$

While  $\mathcal{D}_{planar}$  reflects the dampening effect of gas rarefaction in the absence of boundary curvature,  $\mathcal{D}_{curv}$  combines the impacts of gas rarefaction and geometric reduction on signal decay. As specified by Eq. (48),  $\mathcal{D}_{curv}$  is the product of an  $r^{-1}$  decay rate (characteristic of continuum flow conditions; cf. Eq. (6)) with the  $\left\{ 1 - \exp \left[ -\frac{z_0 r}{3} \left( \sin^{-1}(1/r) \right)^2 \right] \right\}$  component, caused by the narrowing in the volume occupied by the ballistically reflected molecules (see Fig. 1). Indeed, the number of emitted particles that reach a certain distance from the boundary (and therefore contribute to the far acoustic field) is reduced with  $r$ , resulting in a stronger decay rate compared with the planar free-molecular and sphere inviscid setups combined.

The above approximation should be valid at distances  $(r - 1)$  from the source for which  $\omega(r - 1) \gg 1$ . Since the signal at free molecular conditions vanishes at short distances from  $r = 1$ , this requires that the actuation frequency is relatively large. Comparison between our asymptotic and full numerical solutions indicates that the present estimate holds for  $\omega(r - 1) \gtrsim 5$ .

## 5 Numerical scheme: DSMC method

The DSMC method proposed by Bird [44] is a stochastic particle method commonly applied for the analysis of rarefied gas flows. In the present work, the method is used to compute the system acoustic field at arbitrary rarefied-flow conditions, and to validate our analytical ballistic- and continuum-limit solutions. We adopt Bird's algorithm in one-dimensional spherical coordinates, together with the Variable Hard Sphere (VHS) model of molecular interaction [44], to simulate the gas response. To enable comparison between the DSMC and R13 model for Maxwell molecules, the molecular collisional cross section should to be accordingly defined. Towards this end, the Chapman-Enskog value for the dimensional dynamic viscosity of a VHS gas is given by [44]

$$\mu_0^* = \frac{15 \left( \pi m^* k_B^* \right)^{1/2} (4k^*/m^*)^{\varpi-1/2} T_0^{*\varpi}}{8\Gamma(9/2 - \varpi) \Sigma^* u_{rel}^{*2\varpi-1}}, \quad (49)$$

where  $k_B^*$  is the Boltzmann constant,  $m^*$  and  $\Sigma^*$  are the molecular mass and collisional cross section, respectively,  $u_{\text{rel}}^*$  denotes the relative velocity of the molecules,  $\varpi$  marks the viscosity temperature index, and  $\Gamma(\cdot)$  is the Gamma function. Substituting  $\varpi = 1$  for a Maxwell gas, and using the relation  $l_0^* = \mu_0^*/\rho_0^*U_{\text{th}}^*$  for the mean free path of a Maxwell molecule, we obtain

$$\Sigma^* = \frac{m^*U_{\text{th}}^*}{\rho_0^*u_{\text{rel}}^*l_0^*}, \quad (50)$$

exhibiting the required inverse proportion between the collisional cross section and the molecular relative velocity. The number of molecular collisions within a DSMC cell occurring during a timestep  $\Delta t^*$  is then given by the no-time-counter (NTC) scheme [44],

$$\frac{N_c - 1}{2} \frac{n_c^*U_{\text{th}}^*\Delta t^*}{n_s^*r_0^*\text{Kn}}, \quad (51)$$

where it is assumed that the collision probability of all particles in the cell is uniform. Here,  $N_c$  marks the number of molecules in a cell, and  $n_s^*$  and  $n_c^*$  denote the mass densities of simulated and cell molecules, respectively.

In line with the problem statement in Sec. 2, the spherical boundary in the simulation is modeled as fully diffuse, with prescribed radial velocity and heat-flux. Thus, in difference from traditional realizations of gas-wall interactions, the wall temperature is treated as unknown, and application of the heat-flux condition requires modification of the conventional algorithm. In a recent contribution by the authors [27], a non-iterative procedure for the imposition of a heat-flux condition in a DSMC calculation has been presented. The algorithm has been assigned to analyze a one-dimensional cylindrical setup, and is similarly applied in the present work.

To simulate the gas behavior in the semi-confined gas expanse described while restricting a finite computation domain, we placed a stationary and adiabatic spherical boundary in the far field, so that it does not affect the system response. A known problem in DSMC simulations of spherical domains is in the increase in the number of particles with increasing  $r$ , where, for a uniform cell width,  $N_c \propto r_c^{*2}\Delta r^*$ . In cases where the acoustic signal decays slowly with the distance from the source, this causes a vast non-uniformity in the number of particles in each cell, which leads to inaccuracies in DSMC predictions. To overcome this difficulty, the computational domain was divided into non-uniform cell sizes distributed in a geometric series, with a prescribed ratio

between the farthest and closest cell size, denoted by  $\mathcal{R}_{fc}$  [44]. The value of  $\mathcal{R}_{fc}$  was chosen such that the ratio between the largest and smallest number of molecules within a cell did not exceed 20. In each simulation, the one-dimensional computational grid was divided into  $N_{\text{cell}} = 100 - 200$  cells of radial dimension

$$\Delta r_m^* = L^* a^{m-1} \left( \frac{1-a}{1-a^{N_{\text{cell}}}} \right),$$

where  $m = 1, 2, \dots, N_{\text{cell}}$ ,  $L^*$  is the distance between the spherical source and the “fictitious” outer sphere, and

$$a = \mathcal{R}_{fc}^{1/(N_{\text{cell}}-1)}.$$

A timestep of  $\Delta t^* = 0.3 \Delta r_{\text{min}}^* / U_{\text{th}}^*$  was assigned, where  $\Delta r_{\text{min}}^*$  is the size of the smallest cell.

For the harmonic wall excitation studied hereafter, the computation was followed in time until the system has reached its final periodic state. A single run consisted of  $5 \times 10^7$  particles, and 16 realizations were carried out simultaneously to sufficiently reduce the numerical noise in the calculated fields. Each simulation lasted between 12-48 hours (depending on the system Knudsen number and excitation frequency) using a ten-cores Intel i7-6950 machine.

## 6 Results

Focusing on the case of harmonic wall excitations (see Eq. (3)), the system response to vibroacoustic ( $\overline{U}_w = 0.02, \overline{Q}_w = 0$ ) and thermoacoustic ( $\overline{U}_w = 0, \overline{Q}_w = 0.02$ ) input signals is discussed in Secs. 6.1 and 6.2, respectively. The small values of  $\overline{U}_w$  and  $\overline{Q}_w$  are chosen to comply with problem linearization assumed at the outset. In each case we study the long-time periodic system behavior, where the results are presented at half period time,  $t = T/2 = \pi/\omega$ , as a representative time. A comparison is made between the vibroacoustic and thermoacoustic responses, to examine the effectiveness of the latter in reducing vibroacoustic sound.

### 6.1 Adiabatic pulsating sphere

Setting  $\overline{U}_w = 0.02$  and  $\overline{Q}_w = 0$ , we start by examining the effect of slight rarefaction on the deviation from the continuum  $\text{Kn} \rightarrow 0$  inviscid limit given in Eq. (6). Towards this end, Figure 2

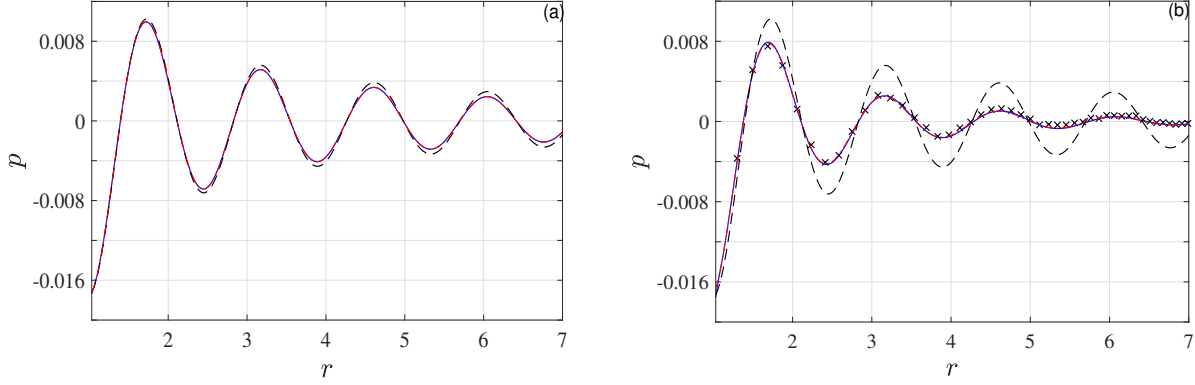


Figure 2: Breakdown of the continuum inviscid solution with increasing  $\text{Kn}$  for an adiabatic pulsating sphere with  $\omega = 4$ : variation of the pressure fluctuation at (a)  $\text{Kn} = 0.0015$  and (b)  $\text{Kn} = 0.015$ . The dashed black, solid blue and dash-dotted red curves show the continuum inviscid ( $\text{Kn} \rightarrow 0$ ), NSF and R13 results, respectively. The crosses mark DSMC predictions. The results are presented at half period time,  $t = T/2 = \pi/\omega$ .

presents the vibroacoustic pressure signal obtained at  $\omega = 4$  and small values of  $\text{Kn} = 0.0015$  (Fig. 2a) and  $\text{Kn} = 0.015$  (Fig. 2b). The inviscid solution is shown by the dashed lines for reference. Due to the exceedingly small value of  $\text{Kn}$  in Fig. 2a, DSMC results are not presented. In this case, the NSF and R13 solutions coincide, and nearly match with the inviscid result. The effect of gas rarefaction becomes more visible in Fig. 2b, where  $\text{Kn}$  is increased by an order of magnitude. While there are still no discrepancies between the NSF and R13 predictions, considerable deviations are observed from the inviscid signal. These are attributed to the added effect of viscosity, which causes a stronger decay rate of the far-field dominating compression wave (see  $\lambda_1$  and  $\lambda_1^{\text{NSF}}$  in Eqs. (23) and (28), respectively). The R13 and NSF fields, showing the vanishing of the pressure signal at nearly six radii away from the source, fully agree with the DSMC results depicted by the crosses. This suggests the continuum-limit solution as a viable means for predicting the system behavior at slightly rarefied conditions, which is particularly useful in view of the relatively slow decay rate of the signal at small  $\text{Kn}$ , and associated exceedingly time consuming DSMC runs.

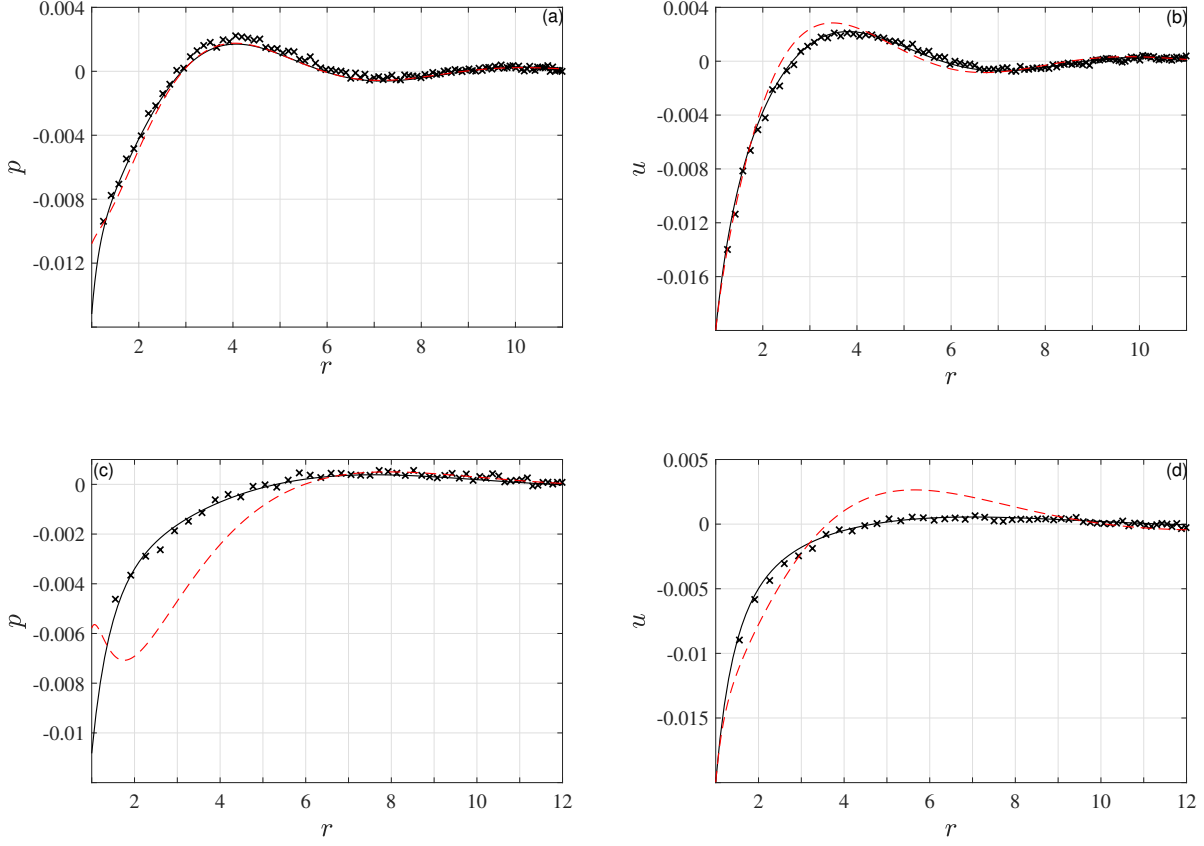


Figure 3: Applicability of NSF (dashed red lines) and R13 (solid black curves) solutions at non-small ( $> 0.1$ ) Knudsen numbers and non-large ( $\leq 1$ ) actuation frequencies for an adiabatic pulsating sphere: comparison with DSMC results (crosses) of the (a,c) acoustic pressure and (b,d) radial velocity fields at (a,b)  $(Kn, \omega) = (0.125, 1)$  and (c,d)  $(Kn, \omega) = (0.5, 0.5)$ . The results are presented at half period time,  $t = T/2 = \pi/\omega$ .

The applicability of the NSF and R13 models at higher Knudsen numbers is inspected in Figure 3, where both acoustic pressure and radial velocity fields are compared with DSMC computations. The  $(\text{Kn}, \omega)$  combinations are chosen so that  $\omega^2 \text{Kn}$ , the leading order decay rate of the compression wave, is fixed (see  $\lambda_1$  and  $\lambda_1^{\text{NSF}}$  in Eqs. (23) and (28), respectively). This is supported by the results, showing that all fields decay at a similar rate away from the source. Recalling that the plots are presented at half period time, the value of  $u = -0.02$  at  $r = 1$  agrees with the impermeability condition at the wall, requiring that  $u = \bar{U}_w$  at  $t = T/2$ .

Comparing between the NSF and R13 results, we observe considerable discrepancies in the higher  $\text{Kn} = 0.5$  case in Figs. 3c and 3d. At this relatively large  $\text{Kn}$ , the effect of the Knudsen layer mode  $\lambda_3$ , missing from the NSF description, becomes dominant, and affects both near- and far-field behaviors. Remarkably, the R13 predictions are in good agreement with DSMC results even at  $\text{Kn} = 0.5$ , where the NSF model is ineffective. Our findings therefore establish that, at relatively non-large excitation frequencies ( $\omega \lesssim 1$ ), the R13 model provides results that are applicable at  $\text{Kn}$  values significantly larger than in the NSF scheme. Specifically, for  $\omega \lesssim 1$ , the calculations indicate that the R13 model is valid up to  $\text{Kn} \approx 0.6$ , while NSF predictions break down already at  $\text{Kn} \approx 0.1$ .

In difference from the extended applicability of the R13 model at  $\omega \lesssim 1$ , the scheme does not improve considerably over the NSF description at higher frequencies. In this case, the problem timescale becomes more restrictive in determining the flow regime, and the transition between the near continuum and intermediate states occurs at lower values of  $\text{Kn}$ . To rationalize the differences between the low and high frequency responses, we expand the near-continuum solution obtained in Sec. 3 in  $\text{Kn}$  and  $\omega$  for  $r \gg 1$ . Each of the hydrodynamic fields then takes the form

$$a_0 O\left(\frac{\omega}{[1 + \omega^2/c_0^2]^{1/2}}\right) + a_1 O(\omega^2 \text{Kn}) + \dots,$$

where  $a_0$  and  $a_1$  are independent of  $\text{Kn}$  and  $\omega$ . The leading order term represents the inviscid solution (see Eq. (6)), and the correction originates from the far-field decay of the compression wave (see the  $\lambda_1$  component in Eq. (25)). At  $\omega \ll 1$ , the leading order is  $O(\omega)$ , which is  $\sim O(\text{Kn}_\omega)$  larger than the  $O(\omega^2 \text{Kn})$  correction. Since  $\text{Kn} \gg \text{Kn}_\omega$  at  $\omega \ll 1$ , the breakdown of the continuum solution is determined by the value of  $\text{Kn}$ . In contrast, for  $\omega \gg 1$ , the inviscid solution

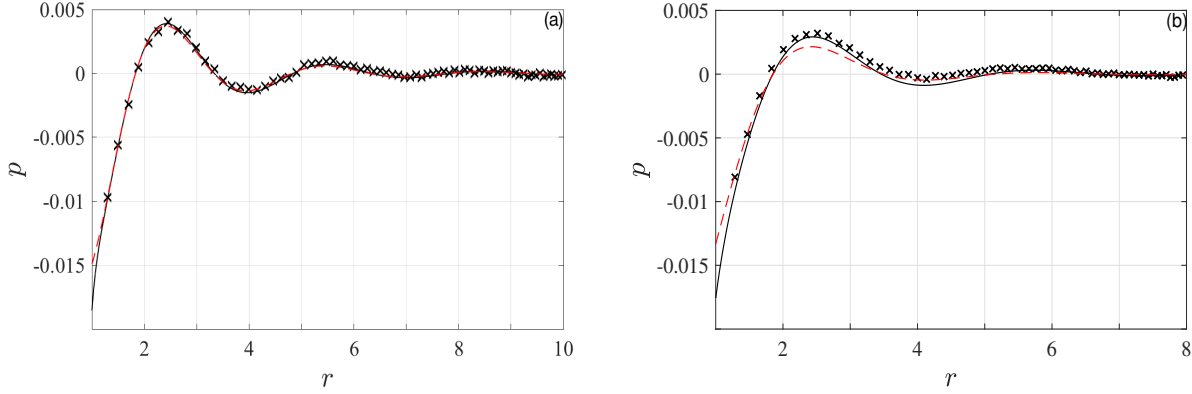


Figure 4: Applicability of NSF (dashed red lines) and R13 (solid black curves) solutions for an adiabatic pulsating sphere with  $\omega = 2$ : comparison of the acoustic pressure with DSMC results (crosses) at (a)  $\text{Kn} = 0.06$  and (b)  $\text{Kn} = 0.125$ . The results are presented at half period time,  $t = T/2 = \pi/\omega$ .

becomes  $O(1)$ , thus  $\sim O(\omega^2 \text{Kn})$  larger than the correction term. For the near-continuum scheme to be effective it is therefore required that  $\omega^2 \text{Kn} = \omega \text{Kn}_\omega \ll 1$ , which restricts the upper limit of Knudsen numbers to decrease as  $\omega^{-2}$ .

To illustrate the breakdown of the near-continuum scheme at non-small frequencies, Figure 4 presents a comparison of the acoustic pressure between the NSF, R13 and DSMC calculations at a fixed  $\omega = 2$  and different values of  $\text{Kn} = 0.06$  and  $\text{Kn} = 0.125$ . While the NSF and R13 results agree with DSMC data at  $\text{Kn} = 0.06$  (corresponding to  $\omega \text{Kn}_\omega = 0.24$ ), they only partially approximate the pressure field at  $\text{Kn} = 0.125$  ( $\omega \text{Kn}_\omega = 0.5$ ), with each matching with a different part of the DSMC signal. In line with the above discussion, the results at this and higher values of  $\omega$  indicate that both the NSF and R13 models break down at an approximately constant value of  $\omega \text{Kn}_\omega \approx 0.3$ , with the R13 approximation not providing improvement over the NSF model. This result may be rationalized by recalling that the differences between the schemes are primarily attributed to the Knudsen layer mode  $\lambda_3$  obtained in Eq. (23), and noting that its decay rate is independent of the excitation frequency (although an increase in  $\omega$  should inevitably lead to the narrowing of the layer). The apparent deficiency in capturing the system high-frequency behavior

may be resolved by reformulating the R13 equations with account taken of the short characteristic time scales. As most of the existing works on moment equations have focused on steady-flow problems [38], such an extension has not been followed hitherto, and may be a topic for future investigation.

Either by increasing  $\text{Kn}$  above  $\approx 0.6$  for  $\omega \lesssim 1$ , or by taking  $\omega\text{Kn}_\omega$  over  $\approx 0.3$  for  $\omega \gtrsim 1$ , the effect of gas rarefaction turns sufficiently strong so that the R13 description breaks down, and the system transits to its intermediate, and, later on, free-molecular regimes. These trends are illustrated in Figure 5. As mentioned in the beginning of Sec. 4, free-molecular conditions should prevail wherever the setup lengthscale or timescale are short compared with the molecular mean free path or mean free time – or, in terms of the problem nondimensional parameters,  $\text{Kn} \gg 1$  or  $\text{Kn}_\omega \gg 1$ , respectively. These conditions are clearly satisfied by the  $(\text{Kn}, \omega)$  combinations in Figs. 5b and 5d, where the free-molecular results agree with DSMC predictions. Intermediate conditions are observed in Figs. 5a and 5c, where neither the R13, nor ballistic solutions, match with DSMC data. In both figures, the ballistic description provides satisfactory results in the vicinity of the wall (where the effect of molecular collisions is minor), while breaking down at larger  $r$ .

Our discussion on the domains of validity of the approximate solutions is summarized in Figure 6, showing a schematic division of the  $(\text{Kn}, \omega)$  plane into zones where the inviscid, NSF, R13 and free-molecular descriptions prevail. For  $\omega \lesssim 1$ , corresponding to cases where  $\text{Kn} \gtrsim \text{Kn}_\omega \gtrsim \omega\text{Kn}_\omega$ , the acoustic flow regime is governed by  $\text{Kn}$ . Here, the inviscid description breaks down at  $\text{Kn} \approx 0.006$ , whereas the NSF model holds up to  $\text{Kn} \approx 0.1$ . The R13 equations remain effective for  $\text{Kn} \lesssim 0.6$ , above which intermediate flow conditions prevail. The free-molecular limit takes place for  $\text{Kn} \gtrsim 5$ . Considering cases where  $\omega \gtrsim 1$  ( $\text{Kn} \lesssim \text{Kn}_\omega \lesssim \omega\text{Kn}_\omega$ ), system rarefaction is governed by the time-scale-based parameters  $\text{Kn}_\omega$  and  $\omega\text{Kn}_\omega$ . Here, our calculations indicate that the inviscid approximation breaks down above  $\omega\text{Kn}_\omega \approx 0.03$  (see Fig. 2), while the NSF and R13 models turn invalid at a common  $\omega\text{Kn}_\omega \approx 0.3$ . The free-molecular regime becomes effective for  $\text{Kn}_\omega \gtrsim 5$ .

To measure the impact of gas rarefaction on the total source strength, Figure 7 presents the



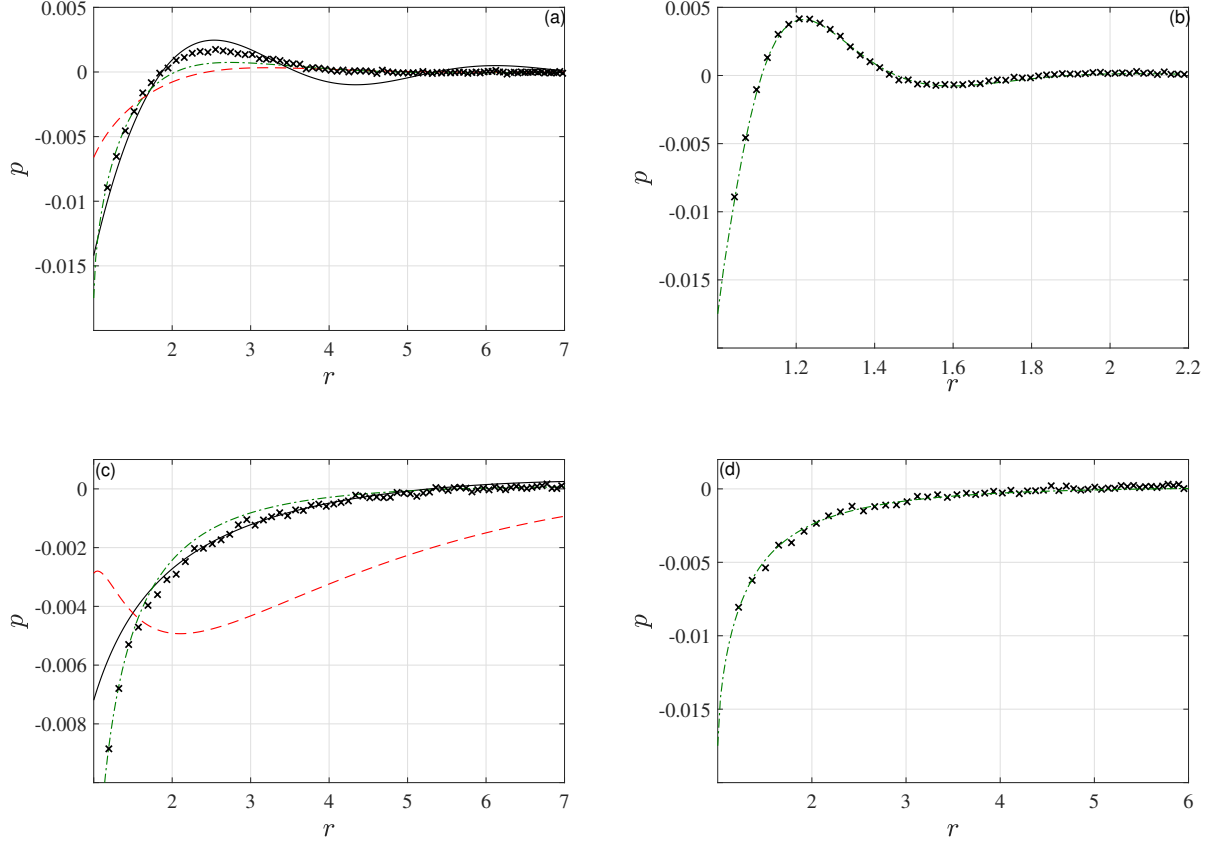


Figure 5: Transition between near-continuum and free-molecular flow regimes for an adiabatic pulsating sphere: comparison between DSMC (crosses), NSF (dashed red lines), R13 (solid black curves), and free-molecular (dash-dotted green lines) solutions for the acoustic pressure at  $(\text{Kn}, \omega)$  combinations of (a)  $(0.5, 2)$ , (b)  $(0.5, 15)$ , (c)  $(2, 0.5)$ , and (d)  $(6, 0.5)$ . The results are presented at half period time,  $t = T/2 = \pi/\omega$ .

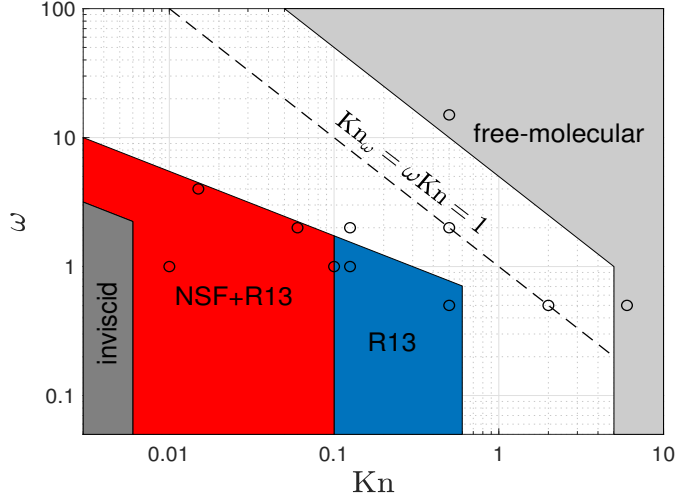


Figure 6: Schematic division of the  $(Kn, \omega)$  plane into domains of validity of the inviscid, NSF, R13 and free-molecular descriptions for an adiabatic pulsating sphere. The  $Kn_\omega = 1$  line marks the locus of points where the excitation frequency is equal to the collision frequency, and the circles denote the parameter combinations considered in Figs. 2-5 and 7.

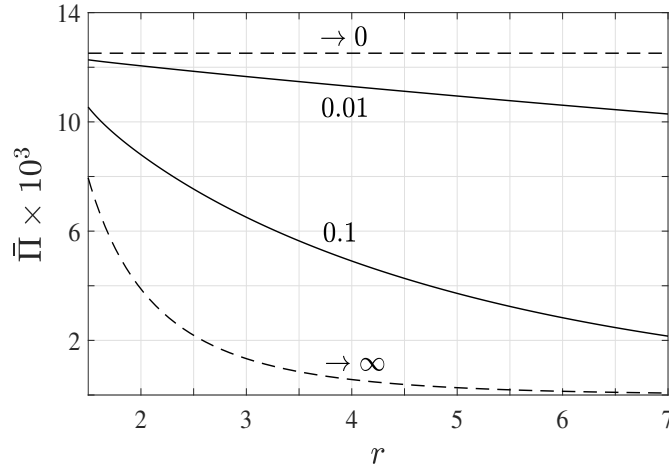


Figure 7: Variation with  $r$  of the time-averaged acoustic power  $\bar{\Pi}$  for an adiabatic pulsating sphere with  $\omega = 1$  and the indicated values of  $Kn$ . The dashed lines show the continuum inviscid ( $Kn \rightarrow 0$ ) and free-molecular ( $Kn \rightarrow \infty$ ) limits, whereas the  $Kn = 0.01$  and  $Kn = 0.1$  curves are obtained from the R13 solution.

effect of the Knudsen number on the time-averaged acoustic power  $\bar{\Pi}$  introduced in Eq. (8). The figure shows the variation of  $\bar{\Pi}$  with  $r$  for  $\omega = 1$  and the indicated values of Kn. The asymptotic inviscid ( $\text{Kn} \rightarrow 0$ ) and free-molecular ( $\text{Kn} \rightarrow \infty$ ) limits are depicted by the dashed lines.

Starting with the inviscid limit, the upper dashed horizontal line in Fig. 7 shows the far-field  $r$ -independent result obtained in Eq. (9). Any viscous effects, manifested by an increase in gas rarefaction, then result in a decrease in the source strength, and in the vanishing of  $\bar{\Pi}(r)$  in the far field. At relatively small Kn, this stems from the stronger than  $1/r$  decay rate of both acoustic pressure and radial velocity, formulated by the exponential  $\lambda_1$  decline of the compression wave in Eq. (25). With further increasing Kn, the acoustic power reduces at a stronger rate away from the source, until in the free-molecular limit it essentially vanishes at  $r \approx 7$ . At a given Kn, the effective distance where  $\bar{\Pi}(r) \rightarrow 0$  diminishes with  $\omega$ . The results for  $\bar{\Pi}(r)$  may be useful in estimating the impact of gas rarefaction on the layer affected by a three-dimensional monopole source.

## 6.2 Heated stationary sphere

We now turn to consider the thermoacoustic problem of a heated stationary surface. Setting  $\bar{U}_w = 0$  and  $\bar{Q}_w = 0.02$ , we first validate the applicability of our approximate solutions by comparison with DSMC data. We then examine the possibility of applying boundary heating to cancel out the vibroacoustic sound caused by wall pulsations. Since most of the results are qualitatively similar to those presented in Sec. 6.1, we focus our presentation on findings that have not been previously discussed.

Figure 8 studies the validity of the NSF, R13 and free-molecular approximations through comparison of the acoustic pressure with DSMC-calculated data. Fixing  $\omega = 0.5$ , different values of  $\text{Kn} = 0.2$  and  $\text{Kn} = 6$  are presented. In line with the schematic map presented in Fig. 6, the R13 and free-molecular approximations are effective at the low and high values of Kn presented, respectively. The NSF solution is invalid in Fig. 8a, as the Knudsen number is too high.

Identifying the qualitatively similar waveforms and decay rates of the vibroacoustic and thermoacoustic signals, it appears of interest to examine the effectiveness of using heating-generated sound to reduce the noise caused by mechanical pulsations. Ideally, a linear

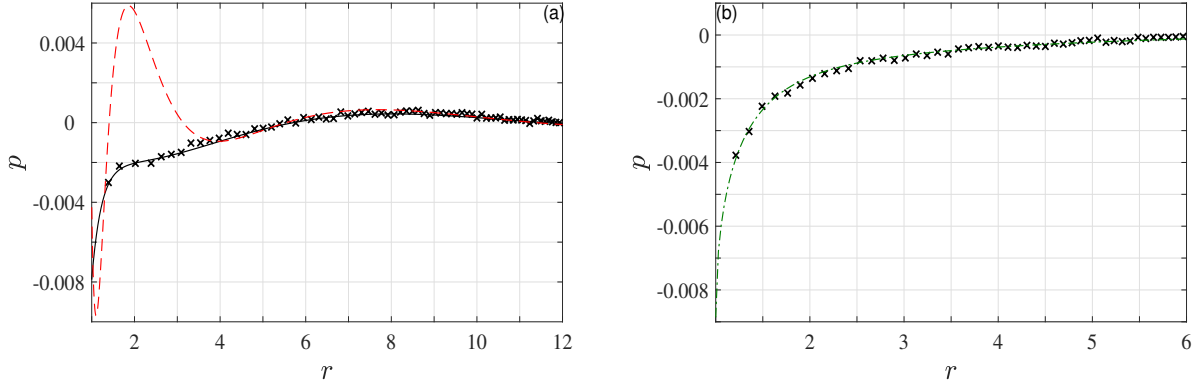


Figure 8: Applicability of NSF (dashed red line), R13 (solid black curve), and free-molecular (dash-dotted green line) solutions for a heated stationary sphere: comparison of the acoustic pressure with DSMC predictions (crosses) at  $\omega = 0.5$  and (a)  $\text{Kn} = 0.2$ , (b)  $\text{Kn} = 6$ . The results are presented at half period time,  $t = T/2 = \pi/\omega$ .

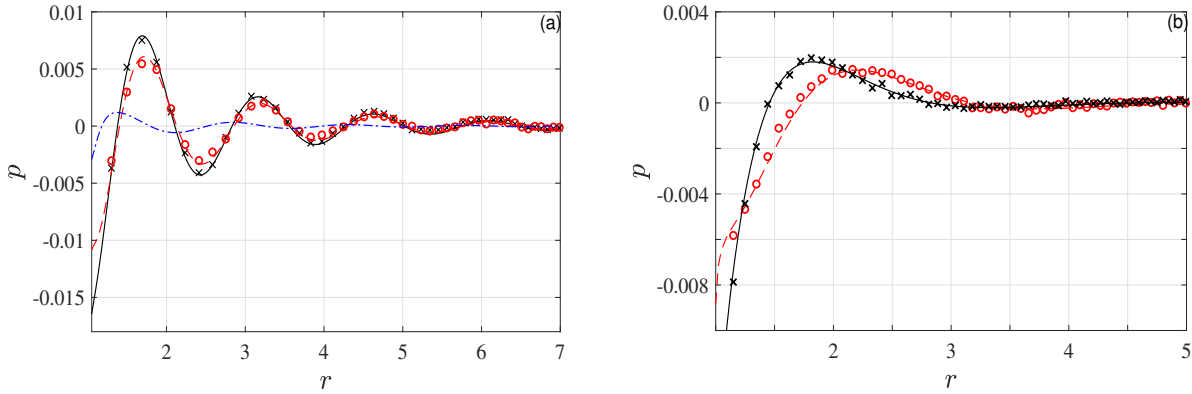


Figure 9: Comparison between the vibroacoustic (black solid lines and crosses) and thermoacoustic (red dashed curves and circles) pressure signals for  $\omega = 4$  and (a)  $\text{Kn} = 0.015$ , (b)  $\text{Kn} = 2$ . The crosses and circles mark DSMC data, the solid and dashed lines in Fig. 9a present R13 results, and the solid and dashed curves in Fig. 9b depict free-molecular approximations. The blue dash-dotted line in Fig. 9a shows the difference between the vibroacoustic and thermoacoustic signals with the latter multiplied by  $\gamma/2(\gamma - 1) = 5/4$ . The results are presented at half period time,  $t = T/2 = \pi/\omega$ .

combination of boundary heating and vibration would result in a moving boundary that generates no sound. Such an approach was followed in the theoretical investigation of a vibrating plane setup [25], which was recently tested in a dedicated experiment combining a thermophone device to generate low-frequency thermoacoustic sound [40]. Applying first-law thermodynamic considerations, it was shown that complete far-field sound cancellation may be achieved at continuum conditions if boundary pulsations and heating are applied at opposite phases and amplitudes ratio of

$$\mathcal{R}_{\text{optimal}} = \left| \frac{\overline{Q}_w}{\overline{U}_w} \right|_{\text{optimal}} = \frac{\gamma}{2(\gamma - 1)} = \frac{5}{4}, \quad (52)$$

where  $\gamma = 5/3$  [25]. At non-continuum conditions, only partial cancellation could be achieved due to the more complex nature of the acoustic signal.

Applying the same approach, Figure 9 seeks to test the conditions at which vibroacoustic sound cancellation may be obtained. Since the thermodynamic considerations made in the planar setup investigation remain unchanged in the spherical configuration, the optimal  $\gamma/2(\gamma - 1)$  ratio should hold for  $\text{Kn} \rightarrow 0$ . This is confirmed by the results in Fig. 9a, indicating that nearly complete sound cancellation is obtained in the far field at  $\text{Kn} = 0.015$  with the above choice of  $\mathcal{R}_{\text{optimal}}$ . The non-zero values observed in the vicinity of the boundary (see the dash-dotted blue line in Fig. 9a near  $r = 1$ ) are mainly attributed to the thermal mode ( $\lambda_2$ ), which contributes to the near-wall pressure at  $\text{Kn} \neq 0$ . These deviations vanish with further decreasing  $\text{Kn}$ . In contrast, in the limit of large gas rarefaction presented in Fig. 9b, the vibroacoustic and thermoacoustic signals appear of different forms, and no single factor multiplication may result in uniform sound cancellation. This is since, at these and other finite Knudsen number conditions, the far-field sound is composed of several acoustic modes, each of which requires different conditions for its cancellation.

## 7 Conclusion

We studied the vibroacoustic and thermoacoustic responses of a gas to small-amplitude normal-to-boundary mechanical and heat-flux excitations of a sphere at rarefied flow conditions. The problem was analyzed in the entire range of gas rarefaction and input frequencies, to characterize

the effect of continuum breakdown on monopole radiation in a three-dimensional setup. Numerical calculations were carried out via the direct simulation Monte Carlo method, and were used to validate analytical predictions in the free-molecular and near-continuum regimes. In the latter, the regularized thirteen moment (R13) equations were applied, to capture the system response at states where the Navier-Stokes-Fourier (NSF) description breaks down. Comparing with the continuum inviscid solution, the results revealed the dampening effect of gas rarefaction on source point-wise strength and acoustic power. At near-continuum conditions, the acoustic field is composed of exponentially decaying “compression”, “thermal” and “Knudsen-layer” modes, reflecting thermoviscous and rarefaction effects. With reducing rarefaction, the contributions of the latter two vanish, and the former mode degenerates into the ideal-flow inverse-to-distance decaying wave. Stronger attenuation was observed with increasing rarefaction, where boundary sphericity results in a “geometric reduction” of the molecular layer affected by the source. Notably, while the R13 model at low frequencies improves over the NSF description at moderate rarefaction levels, both approximations become invalid at common low Knudsen numbers for high frequencies.

While our results have focused on the gas response to harmonic surface excitations, the free-molecular solution in Sec. 4 may be applied for arbitrary small-amplitude input profiles. In addition, the periodic response analyzed in the continuum limit may be considered as a generalized Fourier component forming the gas reaction to any time-dependent input. In this context, the frequency-independent value of  $\mathcal{R}_{\text{optimal}}$  for sound cancellation, stated in Eq. (52) and confirmed by Fig. 9a, may be of practical value to reduce the vibroacoustic noise generated by any input signal at small Knudsen numbers.

Considering the common breakdown of the NSF and R13 descriptions at high frequencies, it may have been argued that a higher-order moment model (e.g., the regularized twenty-six moment equations, R26 [45]) would yield superior results. While this may be true at low frequencies, counterpart improvement is not anticipated at high frequencies. In view of the analysis in Sec. 3, this result may be attributed to the Knudsen layer mode  $\lambda_3$  contained in the R13 solution (see Eq. (23)), and missing from the NSF description. Here, although an increase in  $\omega$  should inevitably lead to the narrowing of the layer, the leading order of the mode decay rate is independent of the excitation frequency. Observing that most of the works on moment equations have focused on

steady-flow problems, it may therefore be worthwhile to reassess these models in setups where short timescales prevail.

## Acknowledgments

This research was supported by the Israel Science Foundation (grant No. 1084/16) and the Aeronautical Engineering Research Fund. Y.B. acknowledges the support by the Adams Fellowship Program of the Israel Academy of Sciences and Humanities.

## A Expressions for the hydrodynamic fields in the R13 solution

In terms of  $\bar{T}(r)$ , the density amplitude function  $\bar{\rho}(r)$  is given by

$$\begin{aligned} \bar{\rho}(r) = & \frac{1}{i\omega\text{Kn} \left[ 1 + \frac{61}{5}i\omega\text{Kn} - \frac{678}{25}(\omega\text{Kn})^2 + \frac{2016}{25}i(\omega\text{Kn})^3 - \frac{2592}{25}(\omega\text{Kn})^4 \right]} \\ & \times \left\{ 9\text{Kn}^4 \left[ 1 + \frac{36}{5}i\omega\text{Kn} \right]^2 \nabla_r^4 \bar{T} \right. \\ & - \frac{15}{4}\text{Kn}^2 \left[ 1 + 18i\omega\text{Kn} - \frac{2592}{25}(\omega\text{Kn})^2 - \frac{5184}{25}i(\omega\text{Kn})^3 + \frac{93312}{625}(\omega\text{Kn})^4 \right] \nabla_r^2 \bar{T} \\ & \left. + \frac{3}{2}i\omega\text{Kn} \left[ 1 + \frac{61}{5}i\omega\text{Kn} - \frac{1218}{25}(\omega\text{Kn})^2 - \frac{2448}{25}i(\omega\text{Kn})^3 + \frac{2592}{25}(\omega\text{Kn})^4 \right] \bar{T} \right\}. \end{aligned} \quad (\text{A1})$$

Assigning  $\bar{T}(r)$  from Eq. (25), we find

$$\bar{\rho}(r) = \sum_{n=1}^3 F_n C_n \frac{\exp[-\lambda_n r]}{r}, \quad (\text{A2})$$

where

$$\begin{aligned} F_n = & \frac{1}{i\omega\text{Kn} \left[ 1 + \frac{61}{5}i\omega\text{Kn} - \frac{678}{25}(\omega\text{Kn})^2 + \frac{2016}{25}i(\omega\text{Kn})^3 - \frac{2592}{25}(\omega\text{Kn})^4 \right]} \\ & \times \left\{ 9(\lambda_n\text{Kn})^4 \left[ 1 + \frac{36}{5}i\omega\text{Kn} \right]^2 \right. \\ & - \frac{15}{4}(\lambda_n\text{Kn})^2 \left[ 1 + 18i\omega\text{Kn} - \frac{2592}{25}(\omega\text{Kn})^2 - \frac{5184}{25}i(\omega\text{Kn})^3 + \frac{93312}{625}(\omega\text{Kn})^4 \right] \\ & \left. + \frac{3}{2}i\omega\text{Kn} \left[ 1 + \frac{61}{5}i\omega\text{Kn} - \frac{1218}{25}(\omega\text{Kn})^2 - \frac{2448}{25}i(\omega\text{Kn})^3 + \frac{2592}{25}(\omega\text{Kn})^4 \right] \right\} \end{aligned}$$

for  $n = 1, 2, 3$ . Substituting  $\bar{\rho}(r)$  into the continuity equation (11), we obtain

$$\bar{u}(r) = i\omega \sum_{n=1}^3 F_n C_n \left[ \frac{1}{r\lambda_n} + \frac{1}{(r\lambda_n)^2} \right] \exp[-\lambda_n r]. \quad (\text{A3})$$

The radial stress amplitude  $\bar{\sigma}(r)$  is then obtained by substitution of Eq. (A3), together with the linearized form of the equation of state in Eq. (14), into the  $r$ -momentum equation (12). This yields

$$\bar{\sigma}(r) = -\frac{1}{2} \sum_{n=1}^3 C_n \left[ 1 + \left( 1 + \frac{2\omega^2}{\lambda_n^2} \right) F_n \right] \left[ \frac{1}{r} + \frac{3}{r^2\lambda_n} + \frac{3}{r^3\lambda_n^2} \right] \exp[-\lambda_n r]. \quad (\text{A4})$$

The heat-flux amplitude  $\bar{q}(r)$  is calculated from the energy balance (13), giving

$$\bar{q}(r) = -\frac{1}{2} i\omega \sum_{n=1}^3 C_n \left( F_n - \frac{3}{2} \right) \left[ \frac{1}{r\lambda_n} + \frac{1}{(r\lambda_n)^2} \right] \exp[-\lambda_n r]. \quad (\text{A5})$$

The constants  $C_{1,2,3}$  are determined through the boundary conditions (18) and (19).

## B Evaluation of $I_n^{(m)}$ , $J_n^{(m)}$ and $K_n^{(m)}$ in Eq. (43)

Substituting Eq. (39) together with Eqs. (1)-(2) in their scaled forms into Eq. (43),  $J_n^{(1)}$  and  $K_n^{(1)}$  contain a double integral of the form

$$J_n^{(1)}, K_n^{(1)} = \text{Re} \left\{ \frac{1}{\sqrt{\pi}} \exp[i\omega t] \int_0^\eta d\vartheta_\xi \int_0^\infty \xi^n \sin \vartheta_\xi \exp \left[ -i\omega x_w(r, \vartheta_\xi)/\xi - \xi^2 \right] d\xi \right\}. \quad (\text{B1})$$

Focusing on a high-frequency  $\omega(r-1) \gg 1$  limit and considering the final time-periodic state of the system, the method of steepest descent may be applied to evaluate the  $\xi$ -integral [46]. This yields

$$J_n^{(1)}, K_n^{(1)} \approx \text{Re} \left\{ 3^{-(1+n)/2} \exp[i\omega t] \int_0^\eta z^{n/2} \left( 1 + \frac{a_1}{z} + \frac{a_2}{z^2} + O(z^{-3}) \right) \sin \vartheta_\xi \exp[-z] d\vartheta_\xi \right\}, \quad (\text{B2})$$

where  $z = 3 \left[ \omega x_w(r, \vartheta_\xi)/2 \right]^{2/3} \exp[i\pi/3] \propto [\omega(r-1)]^{2/3} \gg 1$ , and

$$a_1 = (3n^2 + 3n - 1)/12 \quad \text{and} \quad a_2 = (9n^4 + 6n^3 - 51n^2 - 24n + 25)/288.$$



Applying the method of stationary phase to estimate the  $\vartheta_\xi$ -integral about the stationary phase point  $\vartheta_\xi = 0$ , we find

$$\int_0^\eta z^{n/2} \left(1 + \frac{a_1}{z} + \frac{a_2}{z^2}\right) \sin \vartheta_\xi \exp[-z] d\vartheta_\xi \approx z_0^{n/2} \left(1 + \frac{a_1}{z_0} + \frac{a_2}{z_0^2}\right) \left\{ \frac{3}{2rz_0} \left[1 - e^{-\frac{z_0 r}{3}\eta^2} (1 + O(\eta^2))\right] \right\} \exp[-z_0] \quad (\text{B3})$$

with  $z_0 = 3 [\omega(r-1)/2]^{2/3} \exp[i\pi/3] \gg 1$ , which completes the evaluation of  $J_n^{(1)}$  and  $K_n^{(1)}$  in Eq. (B2). It is easily verified that

$$(J_n^{(2)}, K_n^{(2)}) \approx 2 (J_n^{(1)}, K_n^{(1)}),$$

and that the term  $\sqrt{1 - r^2 \sin^2 \vartheta_\xi}$  appearing in  $I_n^{(m)}$  may be approximated by unity for the leading-order evaluation, to yield

$$I_n^{(m)} \approx J_n^{(m)} \approx K_n^{(m)}.$$

The approximate expressions in Eq. (45) for  $I_n^{(m)}$ ,  $J_n^{(m)}$  and  $K_n^{(m)}$  then follow.

## References

- [1] P. M. Morse, Vibration and Sound, McGraw-Hill, 1948.
- [2] L. Landau, E. Lifshitz, Fluid Mechanics, Pergamon, Reading, MA, 1959.
- [3] F. A. McDonald, G. C. Wetsel, Generalized theory of the photoacoustic effect, Journal of Applied Physics 49 (1978) 2313.
- [4] E. Yariv, H. Brenner, Flow animation by unsteady temperature fields, Physics of Fluids 16 (2004) L95–L98.
- [5] H. Hu, Z. Wang, H. Wu, Y. Wang, Analysis of spherical thermo-acoustic radiation in gas, AIP Advances 2 (2012) 032106.
- [6] H. D. Arnold, I. B. Crandall, The thermophone as a precision source of sound, Physical Review 10 (1917) 22.
- [7] E. Wente, The thermophone, Physical Review 19 (1922) 333.

- [8] H. Shinoda, T. Nakajima, K. Ueno, N. Koshida, Thermally induced ultrasonic emission from porous silicon, *Nature* 400 (1999) 853.
- [9] M. Greenspan, Propagation of sound in five monatomic gases, *The Journal of the Acoustical Society of America* 28 (1956) 644–648.
- [10] N. G. Hadjiconstantinou, A. L. Garcia, Molecular simulations of sound wave propagation in simple gases, *Physics of Fluids* 13 (2001) 1040–1046.
- [11] H. Struchtrup, Resonance in rarefied gases, *Continuum Mechanics and Thermodynamics* 24 (2012) 361–376.
- [12] J. Tamayo, Study of the noise of micromechanical oscillators under quality factor enhancement via driving force control, *Journal of Applied Physics* 97 (2005) 044903.
- [13] I. Bargatin, I. Kozinsky, M. L. Roukes, Efficient electrothermal actuation of multiple modes of high-frequency nanoelectromechanical resonators, *Applied Physics Letters* 90 (2007) 093116.
- [14] J. Iannacci, M. Huhn, C. Tschoban, H. Potter, RF-MEMS technology for future mobile and high-frequency applications: Reconfigurable 8-bit power attenuator tested up to 110 GHz, *IEEE Electron Device Letters* 37 (2016) 1646–1649.
- [15] L. Sirovich, J. K. Thurber, Propagation of forced sound waves in rarefied gasdynamics, *The Journal of the Acoustical Society of America* 37 (1965) 329–339.
- [16] S. K. Loyalka, T. C. Cheng, Sound-wave propagation in a rarefied gas, *Physics of Fluids* 22 (1979) 830.
- [17] N. G. Hadjiconstantinou, Sound wave propagation in transition-regime micro- and nanochannels, *Physics of Fluids* 14 (2002) 802–809.
- [18] A. Manela, G. A. Radtke, L. Pogorelyuk, On the damping effect of gas rarefaction on propagation of acoustic waves in a microchannel, *Physics of Fluids* 26 (2014) 032001.

- [19] Y. Sone, Effect of sudden change of wall temperature in rarefied gas, *Journal of the Physical Society of Japan* 20 (1965) 222–229.
- [20] D. C. Wadsworth, D. A. Erwin, E. P. Muntz, Transient motion of a confined rarefied gas due to wall heating or cooling, *Journal of Fluid Mechanics* 20 (1993) 219–235.
- [21] A. Manela, N. G. Hadjiconstantinou, On the motion induced in a gas confined in a small-scale gap due to instantaneous boundary heating, *Journal of Fluid Mechanics* 593 (2007) 453–462.
- [22] A. Manela, N. G. Hadjiconstantinou, Gas-flow animation by unsteady heating in a microchannel, *Physics of Fluids* 22 (2010) 062001.
- [23] J. Nassios, Y. W. Yap, J. E. Sader, Flow generated by oscillatory uniform heating of a rarefied gas in a channel, *Journal of Fluid Mechanics* 800 (2016) 433–483.
- [24] A. Manela, L. Pogorelyuk, Cloaking via heating: Approach to acoustic cloaking of an actuated boundary in a rarefied gas, *Physics of Fluids* 26 (2014) 062003.
- [25] A. Manela, L. Pogorelyuk, Active noise control of a vibrating surface: Continuum and non-continuum investigations on vibroacoustic sound reduction by a secondary heat-flux source, *Journal of Sound and Vibration* 358 (2015) 20–34.
- [26] D. Kalempa, F. Sharipov, Numerical modelling of thermoacoustic waves in a rarefied gas confined between coaxial cylinders, *Vacuum* 109 (2014) 326–332.
- [27] Y. Ben Ami, A. Manela, Acoustic field of a pulsating cylinder in a rarefied gas: Thermoviscous and curvature effects, *Physical Review Fluids* 2 (2017) 093401.
- [28] Y. W. Yap, J. E. Sader, Sphere oscillating in a rarefied gas, *Journal of Fluid Mechanics* 794 (2016) 109–153.
- [29] M. Pelton, J. E. Sader, J. Burgin, M. Liu, P. Guyot-Sionnest, D. Gosztola, Damping of acoustic vibrations in gold nanoparticles, *Nature Nanotechnology* 4 (2009) 492–495.

- [30] V. Juvé, A. Crut, P. Maioli, M. Pellarin, M. Broyer, N. D. Fatti, F. Vallée, Probing elasticity at the nanoscale: Terahertz acoustic vibration of small metal nanoparticles, *Nano Letters* 10 (2010) 1853–1858.
- [31] A. Crut, P. Maioli, N. D. Fatti, F. Vallée, Acoustic vibrations of metal nano-objects: Time-domain investigations, *Physics Reports* 549 (2015) 1–43.
- [32] R. Marty, A. Arbouet, C. Girard, A. Mlayah, V. Paillard, V. K. Lin, S. L. Teo, S. Tripathy, Damping of the acoustic vibrations of individual gold nanoparticles, *Nano Letters* 11 (2011) 3301–3306.
- [33] H. Grad, On the kinetic theory of rarefied gases, *Communications on Pure and Applied Mathematics* 2 (1949) 331–407.
- [34] H. Struchtrup, M. Torrilhon, Regularization of Grad’s 13 moment equations: Derivation and linear analysis, *Physics of Fluids* 15 (2003) 2668–2680.
- [35] H. Struchtrup, *Macroscopic Transport Equations for Rarefied Gas Flows*, Springer, Berlin, Heidelberg, 2005.
- [36] X. Gu, D. Emerson, A computational strategy for the regularized 13 moment equations with enhanced wall-boundary conditions, *Journal of Computational Physics* 225 (2007) 263–283.
- [37] M. Torrilhon, H. Struchtrup, Boundary conditions for regularized 13-moment-equations for micro-channel-flows, *Journal of Computational Physics* 227 (2008) 1982–2011.
- [38] M. Torrilhon, Modeling nonequilibrium gas flow based on moment equations, *Annual Review of Fluid Mechanics* 48 (2016) 429–458.
- [39] R. Claydon, A. Shrestha, A. S. Rana, J. E. Sprittles, D. A. Lockerby, Fundamental solutions to the regularised 13-moment equations: efficient computation of three-dimensional kinetic effects, *Journal of Fluid Mechanics* 833 (2017) R4.

- [40] S. Julius, R. Gold, A. Kleiman, B. Leizeronok, B. Cukurel, Modeling and experimental demonstration of heat flux driven noise cancellation on source boundary, *Journal of Sound and Vibration* 434 (2018) 442–455.
- [41] A. S. Rana, D. A. Lockerby, J. E. Sprittles, Evaporation-driven vapour microflows: Analytical solutions from moment methods, *Journal of Fluid Mechanics* 841 (2018) 962–988.
- [42] A. F. Beckmann, A. S. Rana, M. Torrilhon, H. Struchtrup, Evaporation boundary conditions for the linear R13 equations based on the Onsager theory, *Entropy* 20 (2018) 680.
- [43] M. N. Kogan, *Rarefied Gas Dynamics*, Plenum, New-York, 1969.
- [44] G. Bird, *Molecular Gas Dynamics and the Direct Simulation of Gas Flows*, Clarendon, Oxford, 1994.
- [45] X. Gu, D. Emerson, A high-order moment approach for capturing non-equilibrium phenomena in the transition regime, *Journal of Fluid Mechanics* 636 (2009) 177–216.
- [46] M. Abramowitz, Evaluation of the integral  $\int_0^\infty e^{-u^2-x/u} du$ , *Journal of Mathematical Physics* (Cambridge, Mass) 32 (1953) 188–192.