

# Supplementary Materials

Probing the mechanisms of morphological evolution and phase selection of intermetallic compounds for impurity-tolerant processing of recycled Al alloys

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## S1 Supplementary alloy preparation

Fig. S1 shows a schematic of how samples for synchrotron X-ray radiography were sectioned from an as-cast 1.2Fe or 2.5Fe alloy ingot. First, the sprue riser on the top of the disk ingot was removed. Then, the edge was machined to remove any surface oxide, and  
5 the disk was cut using wire electro-discharge machining (wire EDM) as indicated by the yellow dashed lines. Foil samples for synchrotron X-ray radiography were then sectioned from the ingot using wire EDM.

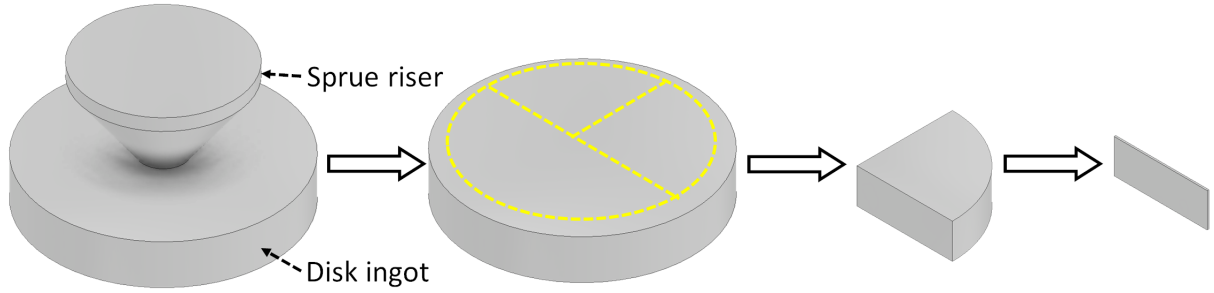
## S2 Supplementary data processing and analysis

As shown in Fig. 3 in the main paper, there is easily resolvable and profound contrast  
10 in the liquid, arising from solute segregation during IMC formation and growth. This

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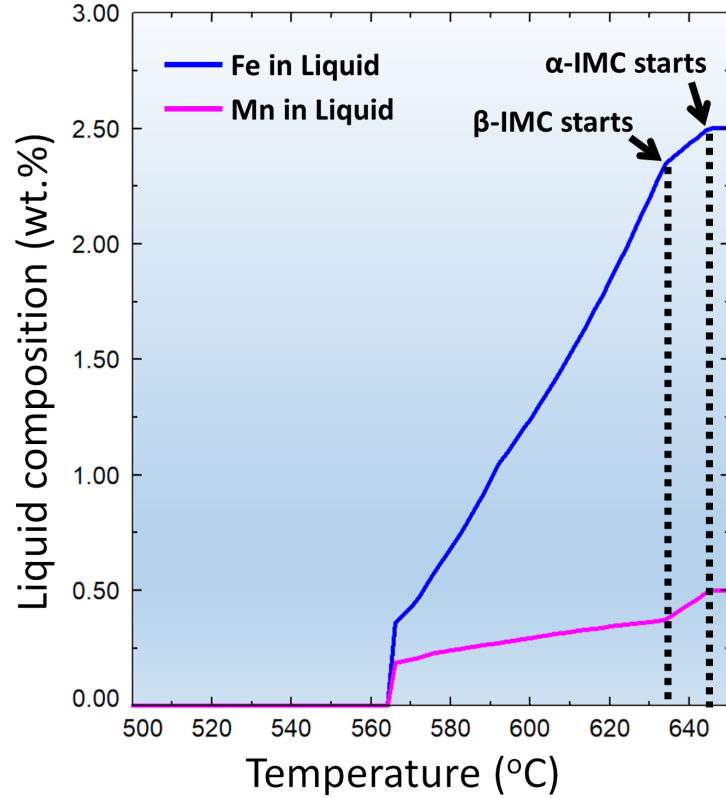
**Figure S1:** A schematic showing how samples for synchrotron X-ray radiography were sectioned from an as-cast 1.2Fe or 2.5Fe alloy ingot.

section describes the procedure followed to allow investigation of the Fe-depleted liquid fraction and its correlation with IMC phase selection in alloy 2.5Fe.

Although the 2.5Fe alloy is a multi-element alloy composed of Al, Si, Mg, Fe and Mn, X-ray absorption by Al, Si and Mg at the beam energy used (pink beam peaking at  
 15 25 keV) is negligible [1]. Further, the total Fe concentration in the liquid is  $> 6$  times larger than Mn concentration (Table 1 in the main paper), and CALPHAD (CALculation of PHase Diagram) simulation in Fig. S2 shows that both Fe and Mn segregate in the same trend during solidification. Therefore, it can be assumed that the X-ray absorption contrast in the liquid is dominated by the segregation (depletion in this case) of Fe. The  
 20 X-ray radiographic images were processed in the following procedure to allow estimation of the Fe-depleted liquid fraction.

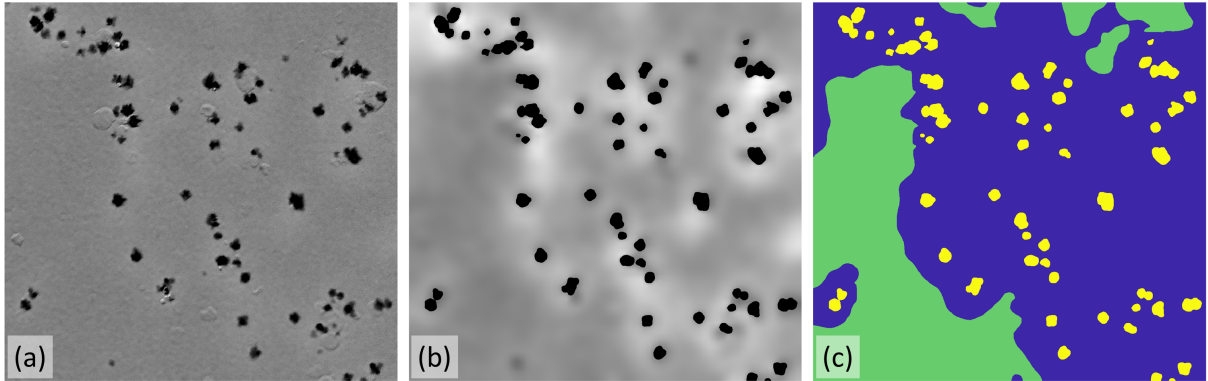
**Flat fielding** First, flat fielding was performed, where each image was divided by a flat image recorded when the sample was fully liquid and uniform. This step removed spatial variations in illumination and static artefacts (e.g. sample surface defects).

25 **Global intensity scaling** To study the evolution of the image intensity field during solidification, a global intensity scaling was performed [2, 3], following the flat fielding, on each image frame. For each experiment, each image frame was normalised between 0 and 1 using a set of global intensity minima and maxima. The global minima and maxima intensities were obtained by scanning through all the frames in the radiography  
 30 sequence. A spatial bilateral filter [4] was then applied on each image for noise reduction



**Figure S2:** Fe and Mn concentrations in the liquid as a function of temperature for alloy 2.5Fe, calculated under equilibrium conditions using FactSage 8.2 and the FTlite database.

while preserving the edges of the IMC crystals (Fig. S3(a)).



**Figure S3:** An example of image processing sequence for evaluation of the Fe depleted liquid fraction. (a) Image after flat fielding and global intensity scaling. (b) Image after segmentation to remove the solid IMC crystals. (c) False colour map after image subtraction by a flat reference image acquired when the sample was in a uniform liquid state. The blue area indicates the Fe-depleted liquid, defined as pixels in the liquid where the greyscale intensity change  $\Delta I > \Delta I^* = 0.03$ .

**Image segmentation** Images were smoothed by applying a diffusion filter [5, 6] and image segmentation was then performed to remove the solid IMC crystals in each frame

(Fig. S3(b)), following a well established procedure presented in details in [1–3, 7]. In Fig. S3(b), the area with a higher intensity (brighter) indicates liquid that was more depleted in Fe.

**Fe depleted liquid fraction** To facilitate the evaluation of the solute depletion effect arising from the interaction between an ensemble of IMCs, image subtraction was performed, where each image was subtracted by a flat reference image acquired before the start of each solidification sequence, with a uniform solute field. The resultant image in Fig. S3(c), with pixel value of  $\Delta I$ , indicated the Fe depletion as the IMC crystals formed:

$$\Delta I = I_i - I_0 \quad (\text{S1})$$

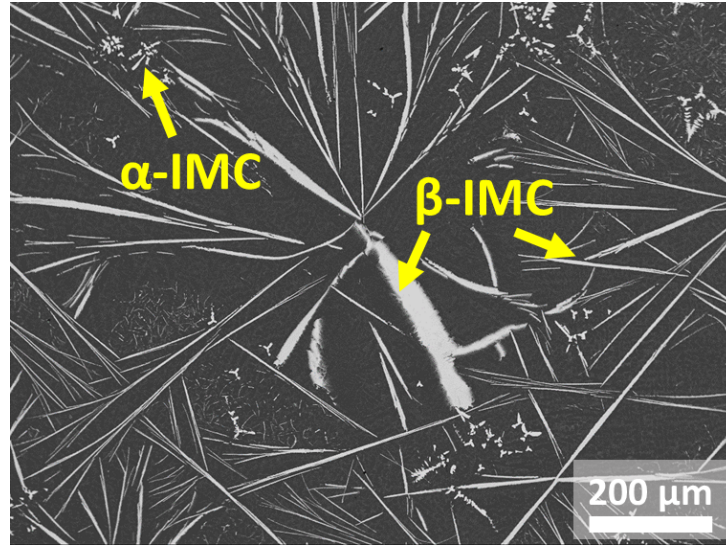
where  $I_i$  is the pixel intensity in the frame of interest, and  $I_0$  is the pixel intensity of the flat reference image. The Fe-depleted liquid was defined as pixels in the liquid where  $\Delta I > \Delta I^* = 0.03$ , and is coloured blue in Fig. S3(c).

### S3 Supplementary results

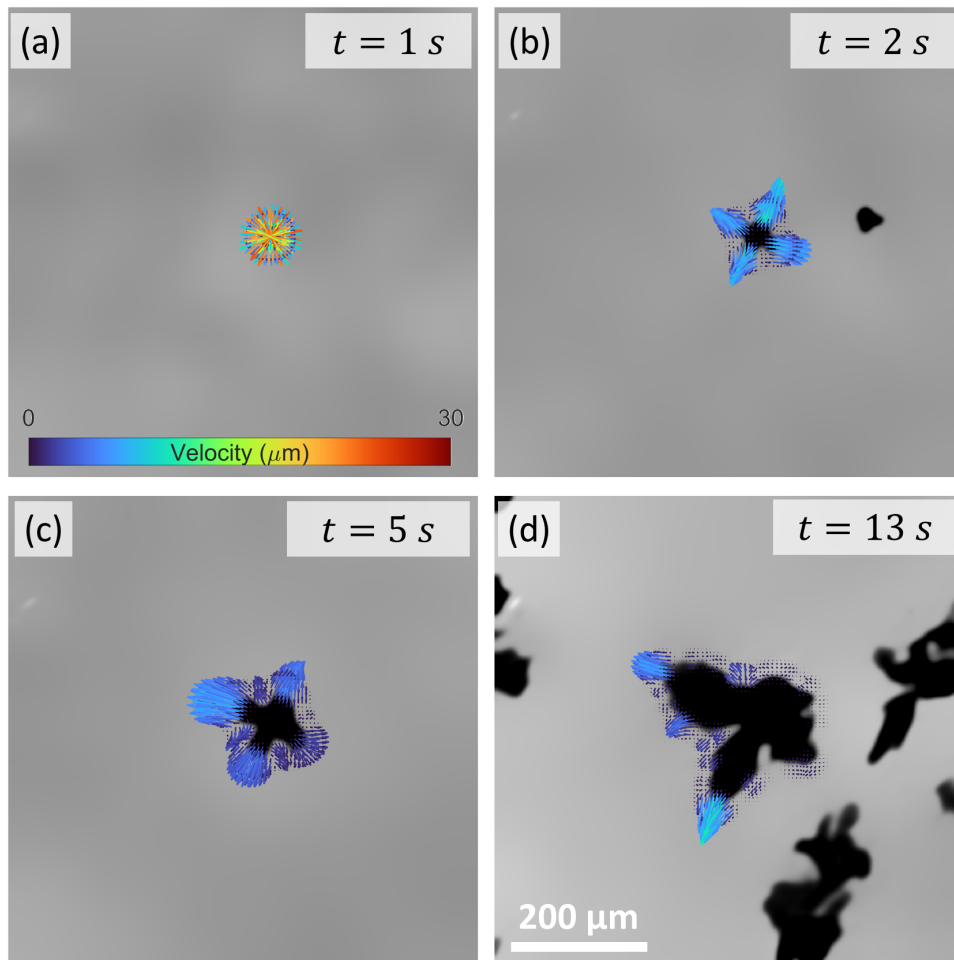
To further study the IMC phase selection in alloy 2.5Fe at higher cooling rates beyond those achievable in the synchrotron rig, a rod sample (8 mm diameter) of the alloy was cast in a water-cooled copper mould (cooling rate  $\sim 100 \text{ K s}^{-1}$ ). Fig. S4 presents the as-cast microstructure, showing  $\beta$ -IMCs as the predominant IMC phase with very few  $\alpha$ -IMCs.

Fig. S5 presents additional radiography sequences superimposed with instantaneous growth velocity fields, showing the growth of non-faceted, dendritic  $\alpha$ -IMC phase in alloy 2.5Fe at  $2 \text{ K s}^{-1}$ .

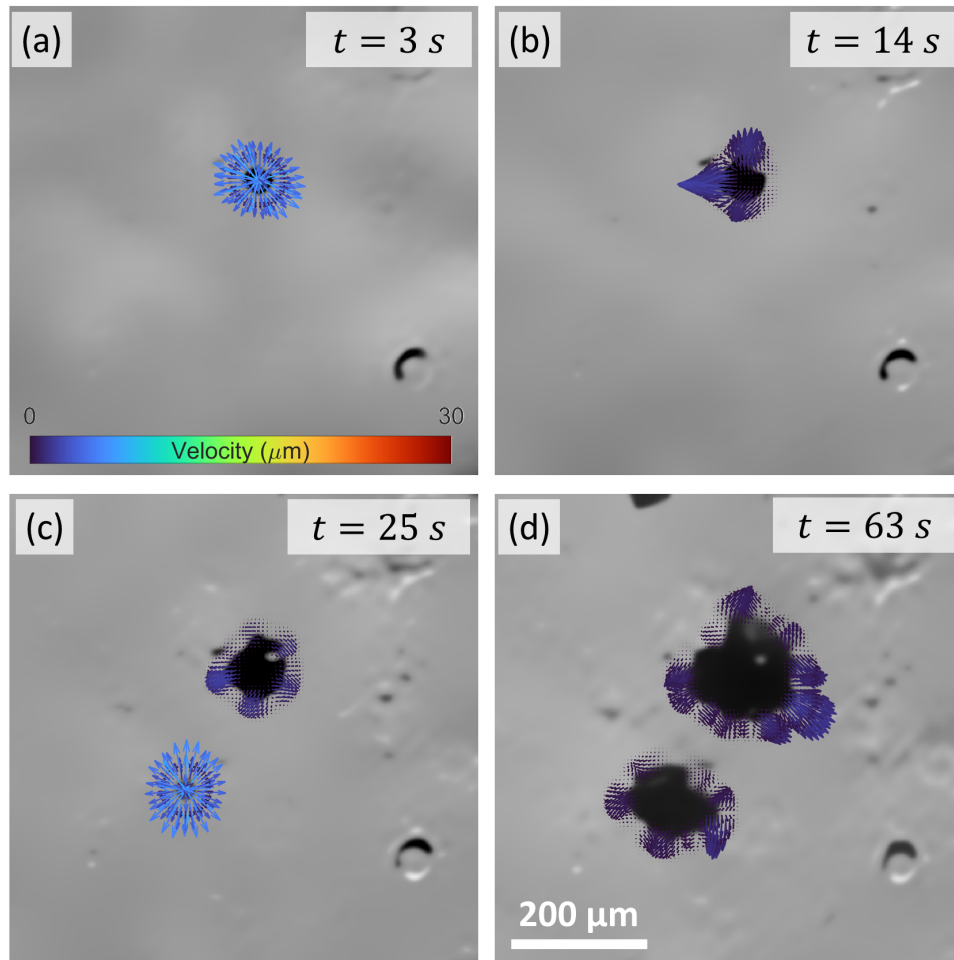
Fig. S6 presents additional radiography sequences superimposed with instantaneous growth velocity fields, showing the growth of faceted, polyhedral  $\alpha$ -IMC phase in alloy 2.5Fe at  $0.5 \text{ K s}^{-1}$ .



**Figure S4:** Microstructure of alloy 2.5Fe cast in a water-cooled copper mould.

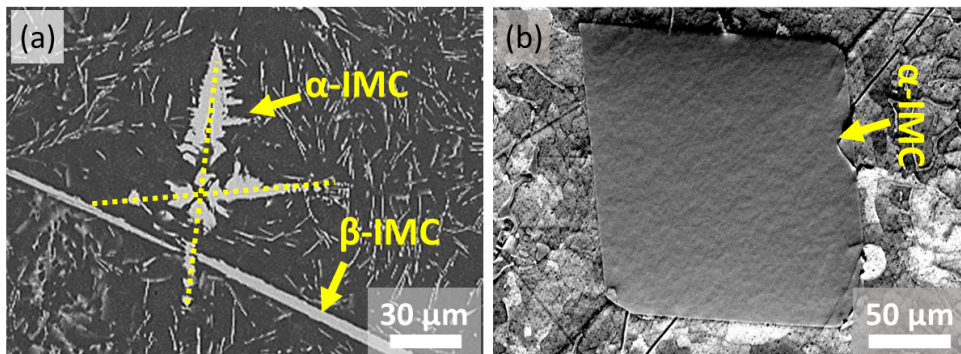


**Figure S5:** Additional radiography sequences superimposed with instantaneous growth velocity fields, showing the growth of non-faceted, dendritic  $\alpha$ -IMC phase in alloy 2.5Fe at  $2 \text{ K s}^{-1}$ .



**Figure S6:** Additional radiography sequences superimposed with instantaneous growth velocity fields, showing the growth of faceted, polyhedral  $\alpha$ -IMC phase in alloy 2.5Fe at  $0.5 \text{ K s}^{-1}$ .

Post-solidification SEM images in Figs. S7(a) and (b) show exposed cross-sections of non-faceted, dendritic and faceted, polyhedral  $\alpha$ -IMCs in alloy 2.5Fe, at  $4 \text{ K s}^{-1}$  and  $0.5 \text{ K s}^{-1}$ , respectively.



**Figure S7:** Post-solidification SEM images showing the exposed cross-sections of (a) non-faceted, dendritic and (b) faceted, polyhedral  $\alpha$ -IMC phase in alloy 2.5Fe, solidified at  $4 \text{ K s}^{-1}$  and  $0.5 \text{ K s}^{-1}$ , respectively. The yellow dashed lines in (a) indicate the primary arms of dendritic  $\alpha$ -IMC.

## 60 **References**

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