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**An *in-situ* powder neutron diffraction study of nano-precipitate formation during processing of oxide-dispersion-strengthened ferritic steels**

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**Abstract**

The evolution of phases in a Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> (wt.%) oxide-dispersion-strengthened ferritic steel during mechanical alloying (MA) and subsequent annealing was studied by high resolution powder neutron diffraction, with emphasis on the kinetics of oxide-based nano-precipitate formation. Y<sub>2</sub>O<sub>3</sub> particles were completely dissolved into the ferritic matrix during MA. The formation of nano-precipitates was then observed by *in-situ* thermo-diffraction experiments during annealing of as-milled powder above 900°C, supported by scanning electron microscopy. This revealed nano-precipitate coarsening with increasing annealing temperature. Powder microhardness was measured at various processing stages, and hardness changes are discussed in terms of the measured phase fractions, crystallite size and lattice strain at different temperatures and times.

**Keywords:** Neutron diffraction; Mechanical alloying; Ferritic steels; Oxide-dispersion-strengthened (ODS) alloy; Precipitation.

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## 1. Introduction

The increasing demand for energy coupled with a need to reduce carbon dioxide emissions associated with fossil fuels has revived interest in nuclear energy, the efficient and safe utilization of which will rely on improved neutron-resistant materials for use in next-generation fission and first-generation fusion power plants. Reduced-activation ferritic oxide-dispersion-strengthened (ODS) steels are promising candidate materials because of their relatively stable high temperature mechanical properties and comparative resistance to neutron irradiation [1]. The superior performance over conventional equivalents is attributed to the presence of nanosized oxide dispersoids that act, even at very low volume fraction (<1 vol%), as: (a) pinning points to dislocation movement giving high temperature strength and creep resistance; (b) nucleation sites for small helium bubbles, preventing formation of large bubbles, or excessive He migration to grain boundaries both of which lead to embrittlement; and (c) stable sinks for irradiation induced defects such as vacancies and interstitial atoms, reducing accumulation of hardening defects such as dislocation loops [1]. Therefore, understanding of oxide-based nano-precipitate (nanocluster) formation during ODS processing is critically important for optimisation of alloy-process combinations.

ODS steels are usually produced by powder metallurgy routes involving mechanical alloying (MA) of  $Y_2O_3$  and pre-alloyed or elemental metallic powders followed by consolidation, such as hot isostatic pressing (HIP) or hot extrusion. The structure and chemistry of the nano-oxide particles in ODS steels have been investigated by using various techniques [2-11], based on which the commonly proposed mechanism for the formation of nano-oxide particles is that room temperature MA produces a supersaturated solid solution containing Y, Ti and O which decomposes during high temperature consolidation to precipitate nano-oxide particles [1]. A

brief review of some key findings that support this mechanism and the remaining uncertainties and limitations of techniques is discussed below.

Cayron *et al.* [2] reported that although  $Y_2O_3$  particles could not be resolved by transmission electron microscopy (TEM) in as-milled Eurofer Fe-9Cr + 0.2 or 1.0 $Y_2O_3$  (mass percent, unless noted otherwise) steel powder,  $Y_2O_3$  particles with a much finer distribution than the starting  $Y_2O_3$  were clearly visible after HIPing. That  $Y_2O_3$  particles are not resolved by TEM in as-milled ODS powder is widely reported, even when a high fraction (3-15%) of  $Y_2O_3$  is added [3,4].

Kimura *et al.* [3] studied the microstructural evolution of Fe-24Cr-15 $Y_2O_3$  during MA and subsequent annealing by X-ray diffraction (XRD) and TEM. It was found that  $Y_2O_3$  particles were gradually fractured, decomposed and finally dissolved into the ferritic matrix at long milling times (360 ks), with milled powder comprising a mixture of elemental Fe, Cr and  $Y_2O_3$ . At the same time, the MA produced ultra-fine (10-15 nm) ferrite grains. After annealing above 1200 K, re-precipitation of both  $Y_2O_3$  and  $YCrO_3$  occurred, which also triggered the growth of matrix grains. Okuda *et al.* [4] showed by small angle X-ray scattering that the  $Y_2O_3$  particles in Fe-13Cr-3Ti-3 $Y_2O_3$  became smaller with the increasing milling time and effectively disappeared after attrition milling for 48 h. They also showed that Ti promoted the dissolution process and more complex Ti-Y-O nano-precipitates ( $Y_2Ti_2O_7$  and  $Y_2TiO_5$ ) were formed during subsequent annealing at temperature above 1273 K.

Miller *et al.* [5,6] and Larson *et al.* [7] studied nanocluster formation in Fe-(12-14)Cr-3W-0.4Ti-0.3 $Y_2O_3$  by atom probe tomography (APT). Neither nanoclusters nor remnants of the

starting  $Y_2O_3$  particles were resolved in as-milled powder. However, in extruded materials, a high number density of Ti-Y-O enriched nanoclusters with a much smaller size (2 nm) than that of starting  $Y_2O_3$  powder (~20 nm) was detected. Their observations supported the hypothesis that  $Y_2O_3$  powder fully dissolves in the ferrite during MA and that there is a thermodynamic preference for Ti-Y-O based compound formation during consolidation. The Y and O concentrations detected by APT in the ferrite matrix from both as-milled Fe-14Cr-2W-0.25Ti-0.2Y-0.05O powder [8] and consolidated Fe-12.3Cr-3W-0.24 $Y_2O_3$ /Fe-12.3Cr-3W-0.39Ti-0.25 $Y_2O_3$  materials [9] were significantly higher than the  $\alpha$ -Fe equilibrium levels, which indicated the formation of a supersaturated solid solution containing Y and O due to the dissolution of  $Y_2O_3$  during MA.

Toualbi *et al.* [10] studied the evolution of  $Y_2O_3$  in Fe-9Cr-10 $Y_2O_3$  powder using neutron diffraction.  $Y_2O_3$  was detected in unmilled powder, but not in 48 h milled powder. After annealing at 1100°C for 1 h and investigation at room temperature, a  $Y_2O_3$  phase re-appeared. Alinger *et al.* [11,12] studied as-milled, annealed and HIPed Fe-14Cr based ODS powder by using small angle neutron scattering (SANS). The nanoclusters were absent in as-milled powder, due to  $Y_2O_3$  dissolution into steel matrix during MA, but re-precipitated in annealed powder at 850°C. These nanoclusters were essentially identical to those in HIP consolidated alloys. Increasing annealing or consolidation temperature resulted in larger nanocluster sizes and smaller number densities and volume fractions.

Zhong *et al.* [13] studied the precipitation kinetics of  $Ti_2Y_2O_7$  nano-precipitates in Fe-14Cr-1W-0.3Ti-0.3 $Y_2O_3$  by SANS and TEM. Ti-Y-O enriched nano-precipitates formed with a very small size of 1.4 nm and volume fraction of 0.4% in as-milled powder. Consolidation by hot extrusion at 1100°C induced slight growth of nano-precipitates to a bimodal particle size

distribution with peaks at 1.4 nm and 5.2 nm. Using X-ray absorption fine structure spectroscopy and TEM, He *et al.* [14] showed a complete dissolution of  $\text{Y}_2\text{O}_3$  in as-milled Fe-13.5Cr-2W-(0-0.4Ti)-0.3 $\text{Y}_2\text{O}_3$  powder.  $\text{Y}_2\text{O}_3$  and  $\text{YCrO}_3$  coexisted in the Ti-free HIPed alloys with Ti-Y-O oxides in HIPed alloys containing Ti, suggesting that the addition of Ti did not facilitate  $\text{Y}_2\text{O}_3$  dissolution, but changed the morphology and chemistry of nano-precipitates in consolidated alloys.

While this brief review shows progress in understanding the dissolution and re-precipitation of nanoclusters, most of the prior studies are limited by two factors:

- 1) They are based on *ex-situ* characterization of the final material at the end of a multi-step consolidation process, so that the details of the early stages of nano-precipitate formation are impossible to recover;
- 2) The characterization techniques study only an extremely limited volume of material, so that representative behaviour is difficult to obtain and nano-scale variations in local chemistry could dominate the observed precipitation behaviour.

In this paper, we use high resolution powder neutron diffraction to study the progressive dissolution of  $\text{Y}_2\text{O}_3$  during MA and then the earliest stages of *in-situ* nano-precipitate formation. Neutron powder diffraction was performed at the ISIS neutron source at Rutherford Appleton Laboratory, UK, using a High Resolution Powder Diffractometer (HRPD). We performed real-time thermo-diffraction experiments on powder samples, milled by various routes, over a wide temperature range, up to a maximum temperature of 1100°C. The penetration depth of neutrons (~25 mm for iron-based alloys) [15] is much larger than

that ( $\sim 5 \mu\text{m}$ ) of X-rays [16], and allows more representative insights of fine-scale microstructural evolution. Specimens for neutron diffraction were the unconsolidated feedstock and milled powders directly, and so no artefacts were introduced during sample preparation or due to consolidation effects. Because the nano-precipitates formed by annealing the as-milled powders in vacuum are almost identical to those formed at the same temperature but under pressure during HIP consolidation routes [11], we expect that this *in-situ* annealing of the MA powder at temperatures between  $800^\circ\text{C}$  and  $1100^\circ\text{C}$  can be used as an analogue to study evolution of the oxide clusters and particles during the HIP process itself. However, the standard  $\text{Y}_2\text{O}_3$  content ( $<0.5\%$ ) in ODS alloys is too small to be detected and analysed with confidence by diffraction-based techniques and therefore a higher  $\text{Y}_2\text{O}_3$  concentration (10%) was used to prepare Fe-14Cr-10 $\text{Y}_2\text{O}_3$  ODS powder. As we show, even at such high loadings, complete dissolution during MA was achieved. To support diffraction data, annealed powder was also examined by high magnification scanning electron microscopy (SEM) to reveal the nano-precipitates. The evolution of powder microhardness and microstructure during MA and subsequent  $\text{Y}_2\text{O}_3$  re-precipitation are also presented and the changes in hardness are rationalized in terms of the phase fractions present, the degree of cold work and the extent of annealing.

## 2. Experimental

ODS ferritic steel powder with nominal composition Fe-14Cr-10 $\text{Y}_2\text{O}_3$  was prepared by MA from a mixture of Ar gas-atomized pre-alloyed Fe-14Cr powder ( $<150 \mu\text{m}$ , Aubert & Duval, France) and  $\text{Y}_2\text{O}_3$  powder, ranging in diameter between 20 nm and 40 nm (Pi-Kem Ltd, UK) in high purity (99.999%) Ar. MA was performed in a planetary mill (Pulverisette 6, Fritsch GmbH, Germany) using a chrome steel bowl (500 ml) and steel balls (400g, 10 mm in



diameter) at a rotational speed of 250 rpm with a ball-to-powder weight ratio of 10:1. Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder subjected to MA reached a steady microstructural condition after 60 hours of MA, as judged by neutron diffraction measurements (see section 3.1). Powders were then annealed at various temperatures in the HRPD to study the kinetics of nano-precipitate formation.

The neutron diffraction measurements used 15 g of powder in a vanadium can under vacuum ( $< 5 \times 10^{-4}$  mbar) placed in the *in-situ* furnace. Powder milled for different times was investigated by neutron diffraction at room temperature and then during annealing at different temperatures between 800 and 1100°C ( $\pm 2^\circ\text{C}$ ) for 1 h. The can was heated at a constant rate of 15°C/min. Diffraction data were collected from the powder in back-scattering mode over a 0.085-0.390 nm range in *d*-space both at high temperature and after cooling to room temperature. Crystallite size and lattice strain were determined from diffraction patterns of both as-milled and annealed powder at room temperature, using Williamson-Hall methods via Rietveld refinement, as programmed in the GSAS suite [17,18].

Annealed powders were mounted with epoxy resin, polished, and etched with 3:1:1 ratio of hydrochloric, nitric and acetic acid for 15 seconds. The microstructures of cross-sections were observed by field emission SEM (JSM-840F). The average size of the nano-precipitates was determined by the mean linear intercept method from at least three SEM images in each case, with more than a hundred particles in each image.

Diamond pyramid hardness measurements (minimum 10 per condition) were performed at room temperature on as-milled and annealed powders using a Vickers microhardness tester

(Model 401/402MVD, Wilson Instruments, USA) at a load of 25 g for 20 s on powder cross-sections polished to a 0.04  $\mu\text{m}$  finish using colloidal silica.

### 3. Result and discussion

#### 3.1 Neutron diffraction of Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder during MA and in-situ annealing

The crystal structure evolution of Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder as a function of milling time according to neutron diffraction is shown in Fig. 1, with diffraction data from the starting pre-alloyed Fe-14Cr and Y<sub>2</sub>O<sub>3</sub> powders included for reference. The two most intense Y<sub>2</sub>O<sub>3</sub> peak positions from as-supplied Y<sub>2</sub>O<sub>3</sub> were at  $d = 0.187$  and  $0.306$  nm, and are indicated by the vertical lines. The mixed but not milled Fe-14Cr + Y<sub>2</sub>O<sub>3</sub> powder (0 h milled) showed diffraction peaks from both bcc ferrite and cubic Y<sub>2</sub>O<sub>3</sub>, and there was a progressive decrease in peak intensity and increased peak broadening for both phases as milling time increased. The peak broadening can be attributed to the well-known effects of decreasing crystallite size and increasing lattice strain, arising from crystal defects accumulated during the cold work associated with MA [19]. Even with 10 wt%, the Y<sub>2</sub>O<sub>3</sub> diffraction peak disappeared almost completely after 12 h milling. It was possible that at this stage undissolved Y<sub>2</sub>O<sub>3</sub> particles may have remained in the microstructure but were now simply too small to be detected [16]. However, after 60 h there were no resolvable Y<sub>2</sub>O<sub>3</sub> peaks, which we assume to be a consequence of the Y<sub>2</sub>O<sub>3</sub> particles being dissociated and finally dissolved in the Fe-14Cr matrix [11]. Segregation of Y dissociated from Y<sub>2</sub>O<sub>3</sub> during MA might be expected to be concentrated at grain boundaries, but Y segregation to the many dislocations in such a highly strained material can also be expected. Atom probe studies (the only true atomic resolution microscopy) have recently confirmed the formation of a relatively *homogeneous*

supersaturated solid solution containing Y and O with extremely low levels of grain boundary segregation, and supporting the relatively homogeneous dissolution of  $Y_2O_3$  during mechanical alloying [6]. Compared with atom probe tomography (or transmission electron microscopy) of as-milled powders, the present paper samples many orders of magnitude higher volumes of material, and shows for the first time important consistency between high resolution but time-consuming studies on tiny volumes of materials and this more representative and faster study by neutron diffraction. The thermodynamic driving force for  $Y_2O_3$  dissolution is an overall reduction of the free energy provided by a single solution of Fe-Cr-Y-O over a highly defective ferritic matrix containing fine  $Y_2O_3$  particles with an increasing interfacial energy as milling progresses [3]. Kinetically, the dissolution into the ferrite is facilitated by small crystallite sizes and a high vacancy and dislocation density [20,21].

When the yttrium and oxygen atoms from disassociated  $Y_2O_3$  were dissolved substitutionally and interstitially in the bcc crystalline lattice of ferrite during MA, distortion of the lattice might be expected because of the atomic misfit between Y and Fe (atomic radius: Y = 0.182 nm; Fe = 0.124 nm) [3]. However, there was no discernible shift in the ferrite peak positions in Fig. 1. Similar results have been previously reported [3,10,22,23], and the comparative insensitivity of the lattice parameters can be attributed to:

1) Any increase in lattice parameter of as-milled powder induced by dissolved Y and O is partially relieved by a decrease in lattice parameter induced by the formation of a high concentration of lattice vacancies during long-time MA [23]; and

2) The diffraction peaks of ferrite from as-milled powder were significantly *broadened* due to decreasing crystallite size and increasing lattice strain, and this makes any underlying peak shifts very difficult to identify [19].

Fig. 2 shows the *in-situ* high temperature neutron diffraction traces of the Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> MA powder after annealing for 1 h at various temperatures in the range 800 - 1100°C. Three room temperature traces are also included for comparison: the upper two patterns from MA powder with milling times of 0 h and 60 h; and a lower pattern from powder annealed at 1100°C for 1 h and cooled to room temperature. The powder annealed at 800°C for 1 h showed no marked change from the as-milled powder, whereas at 900°C an fcc austenite peak developed. Since the nominal 14 wt% Cr content was higher than the minimum of 12.7 wt% [24] required for a fully ferritic microstructure at all temperatures of interest, the formation of austenite might be attributed to the presence of background carbon and nitrogen austenite stabilisers accumulated from the atomisation and ball milling steps [25]. Re-precipitation of Y<sub>2</sub>O<sub>3</sub> also started at 900°C as shown by the broad peaks at  $d \sim 0.187$  and 0.306 nm, the intensity of which increased with increasing annealing temperature above 1000°C. YCrO<sub>3</sub> was also formed above 1000°C, and was consistent with coexistence with Y<sub>2</sub>O<sub>3</sub> above 1300 K as shown in the ternary Y-Cr-O phase diagram [26]. Any high temperature austenite fully transformed to ferrite on cooling, and both Y<sub>2</sub>O<sub>3</sub> and YCrO<sub>3</sub> were retained. There was a shift in diffraction peak position for Y<sub>2</sub>O<sub>3</sub> precipitates and the matrix ferrite toward higher  $d$  values in comparison with unmilled powder because of thermal residual strains.

Since re-precipitation of  $\text{Y}_2\text{O}_3$  started at  $900^\circ\text{C}$ , re-precipitation kinetics as a function of time during isothermal annealing at  $900^\circ\text{C}$  were studied, with powder neutron diffraction patterns recorded repeatedly at 5 min intervals. A selection of the patterns is shown in Fig. 3, again with the patterns for 0 h and 60 h as-milled powder for comparison. Austenite was first resolved after 50 min and re-precipitation of  $\text{Y}_2\text{O}_3$  was first resolved after 60 min. The peak intensity for austenite and  $\text{Y}_2\text{O}_3$  increased with annealing time, and was then unchanged after 120 min at  $900^\circ\text{C}$ . At  $1000^\circ\text{C}$ , nano-precipitate formation was much more rapid and after only 5 min the patterns resembled those for 60 min at  $900^\circ\text{C}$ . Consequently, the temperature range  $900\text{--}1000^\circ\text{C}$  is the practical range for re-precipitation control, with precipitation kinetics spanning approximately an order of magnitude across this interval.

### 3.2 Precipitate morphology

Cross-sectional secondary electron SEM images of etched surface from Fe-14Cr-10 $\text{Y}_2\text{O}_3$  powders annealed at different temperatures ranging from  $800$  to  $1100^\circ\text{C}$  for 1 h are shown in Fig. 4. No features or precipitates (except pores) were resolved after annealing at  $800^\circ\text{C}$ , as shown in Fig. 4(a). Fig. 4(b) shows that annealing at  $900^\circ\text{C}$  led to the formation of 5-50 nm particles, with an average diameter of 10 nm. As the neutron diffraction patterns in Fig. 2 and 3 showed  $\text{Y}_2\text{O}_3$  at  $900^\circ\text{C}$ , these precipitates are likely to be  $\text{Y}_2\text{O}_3$ . Fig. 4(c) shows powders annealed at  $1100^\circ\text{C}$  for 1 h with a much higher fraction of precipitates (an average diameter of  $\sim 25$  nm); here neutron diffraction indicated the presence of  $\text{Y}_2\text{O}_3$  and  $\text{YCrO}_3$ .

### 3.3 Microhardness, crystallite size and lattice strain of powder during processing

Figure 5 correlates changes in microhardness, crystallite size and lattice strain of the Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder with milling time and annealing temperature. Although there are likely to be errors induced by the curve-fitting process in the absolute values of crystallite size and lattice strain, the trend of changes with process conditions was consistent and monotonic. During the early stages of milling (< 12 h), the microhardness of MA powder increased rapidly with milling time, and can be ascribed to a reduction of grain size and increasing work hardening, as evidenced by the decrease in crystallite size and increase in lattice strain in Fig. 5(a). Beyond 12 h, microhardness increased only slowly, reaching a plateau of 771 kg/mm<sup>2</sup> after 60 h. The stability of microhardness corresponded to the gradual stabilisation of both crystallite size at ~ 20 nm and lattice strain at ~ 0.89% after 30 h. We propose that the defect or dislocation density in the powder had stabilised at this stage because a quasi-equilibrium had been established between the rate of dislocation accumulation (work hardening) and rate of thermally induced recovery [27]. Fig. 5(b) shows the variation of microhardness, crystallite size and lattice strain of the Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder after 60 h MA and annealing at different temperatures for 1 h. In general, the crystallite size increased, and the microhardness and lattice strain decreased with increasing annealing temperature. Compared with the 60 h as-milled powder, powder annealed at 800°C had a slightly higher microhardness (816 vs 771 kg/mm<sup>2</sup> for as-milled powder), almost the same crystallite size (~20 nm), but much smaller lattice strain (0.41% vs 0.89% for as-milled powder). The reduction in lattice strain is likely to be associated with recovery/recrystallization processes, as reported for both powder and HIPed Fe-14Cr-0.25Y<sub>2</sub>O<sub>3</sub> processed at similar temperatures [28]. We suggest that the high hardness in as-milled powder, even after annealing at 800°C for 1 h, arises because:

1) The hardness of MA powder after annealing mainly depends on the crystallite size rather than the lattice strain [27]; and

2) Although no nano-precipitates were detected at 800°C (Fig. 2), extremely fine ( $< 5$  nm) nanoclusters may have already started to form, as suggested by recent small angle neutron scattering and atom probe tomography studies on ODS ferritic steels [8,12].

Above 800°C, oxide nano-precipitates were detected by neutron diffraction and their coarsening started as evidenced by SEM images in Fig 4. The crystallite size of annealed powder increased dramatically with increasing annealing temperature and was up to 272 nm for powder annealed at 1100°C for 1 h. Crystallite sizes of up to 1000 nm have been reported previously in powders produced by MA on the basis of HRPD data performed on the same diffractometer [29], which agreed with crystallite data obtained by XRD from the same powder. Therefore, crystallite sizes up to 272 nm obtained from neutron line-broadening data in this work are well within the range of the technique. Obviously, re-precipitation of nano-oxides coincided with the growth of matrix grains [3], and the coarsening of both matrix grains and nano-precipitates gives rise to lower values of powder microhardness.

The change in crystallite size from approximately 20 to 272 nm in Fig. 5(b) did not produce a large decrease (only 25%) in hardness, as might be expected from the “normal” Hall-Petch relationship, because *nanocrystalline* materials very often show decreased microhardnesses when compared with predictions of Hall-Petch type relationships that are obtained for much coarser-grained materials [30].

In summary, this work reveals insights into both the kinetics of  $Y_2O_3$  dissolution and the very beginning of its re-precipitation as nanoclusters, for the first time based on bulk information from ODS powders using *in-situ* high resolution powder neutron diffraction. The nucleation of nano-precipitates started at 800-900°C and significant coarsening started only above 900°C, providing information on the processing window for controlled nano-precipitate size and density, and thus the performance of ODS steels.

#### 4. Conclusions

Microstructural evolution and its relationship with hardness (related to yield strength) in Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> ODS ferritic steel powder during MA and subsequent annealing were studied using neutron diffraction, microscopy and microhardness indentation. Y<sub>2</sub>O<sub>3</sub> particles were gradually fractured and eventually, after 60 hours milling, almost fully dissolved into the ferrite matrix during MA. The subsequent precipitation and formation of nano-size oxide precipitates were successfully observed for the first time by *in-situ* powder neutron diffraction. Although a very fine-scale, low fraction precipitation of oxide could not be excluded at 800°C, distinct precipitation of Y<sub>2</sub>O<sub>3</sub> was first resolved after 1 h at 900°C, along with the coexistence of YCrO<sub>3</sub> and Y<sub>2</sub>O<sub>3</sub> at annealing temperatures of 1000°C and above. Microscopy of annealed powders confirmed coarsening of nano-precipitates with increasing annealing temperature. Powder microhardness variations have been rationalised in terms of the changes in phase, lattice strain, crystallite and nano-precipitate size evolution during annealing.

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**Figure captions**

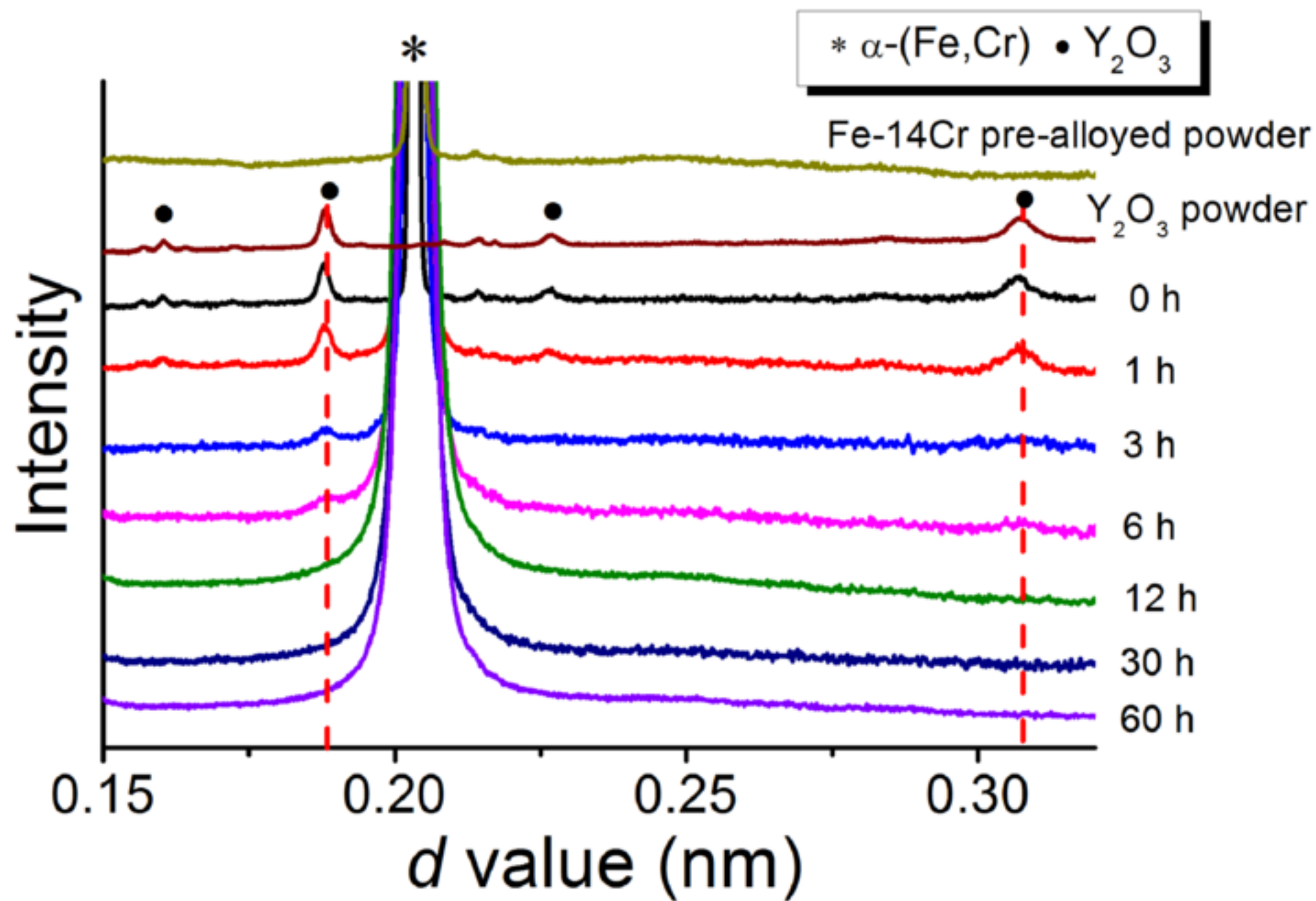
Fig. 1 Neutron diffraction patterns of Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder as a function of MA times.

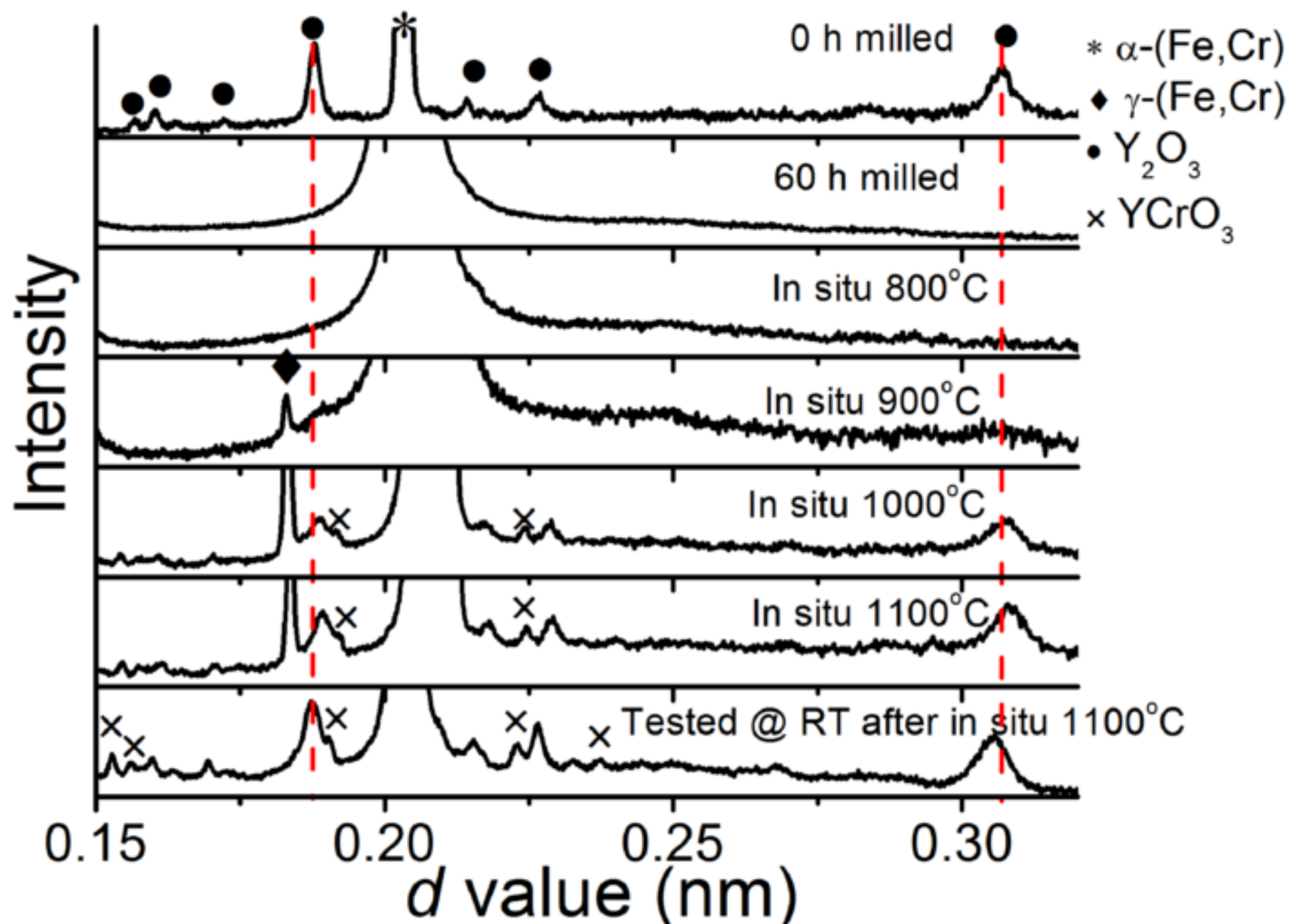
Fig. 2 *In-situ* neutron diffraction patterns of Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder measured during annealing at different temperatures for 1 h.

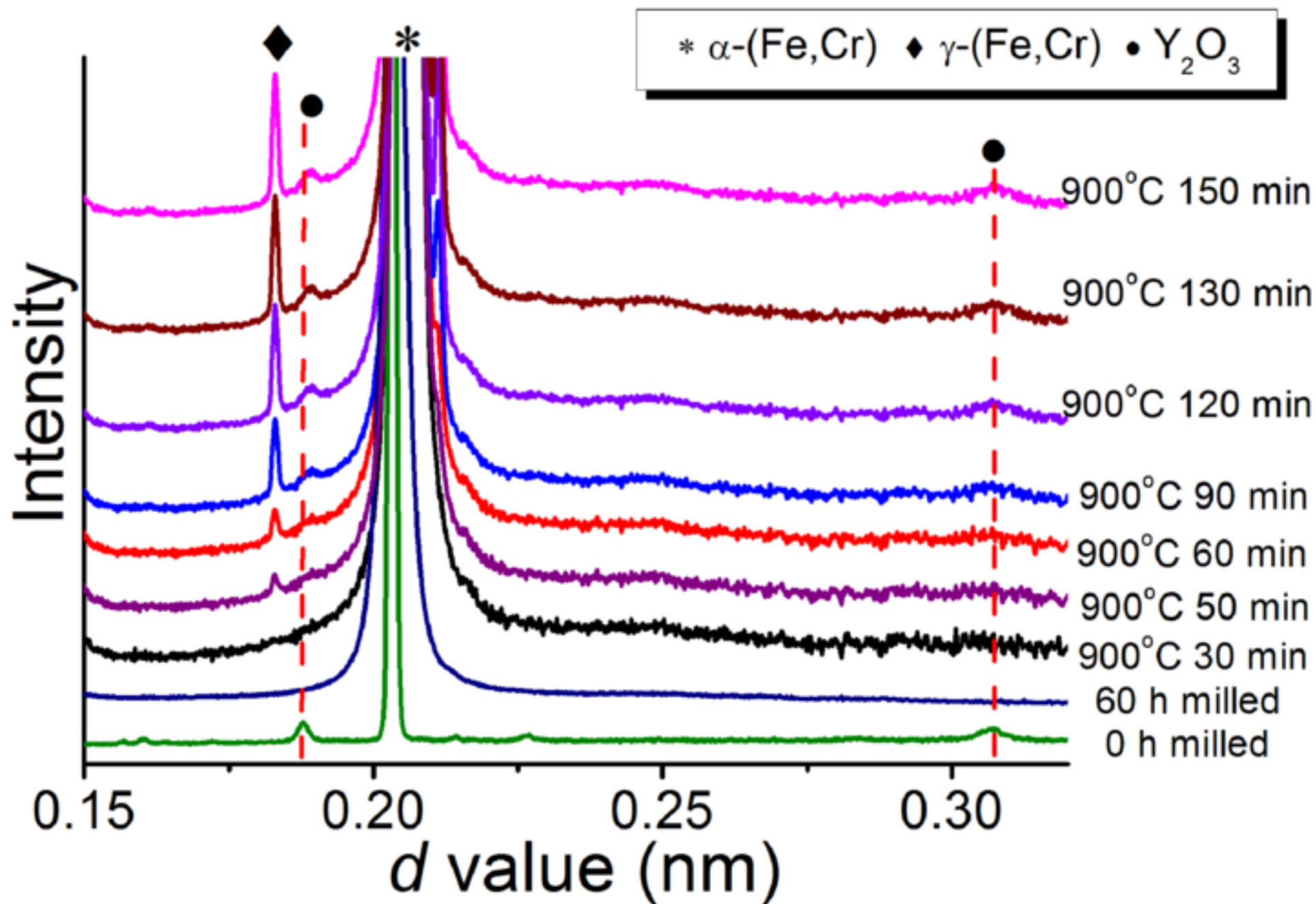
Fig. 3 *In-situ* neutron diffraction patterns of Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder measured during 900°C annealing at different times.

Fig. 4 SEM images of polished and etched surfaces from Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder annealed at different temperatures for 1 h: (a) 800°C; (b) 900°C; and (c) 1100°C.

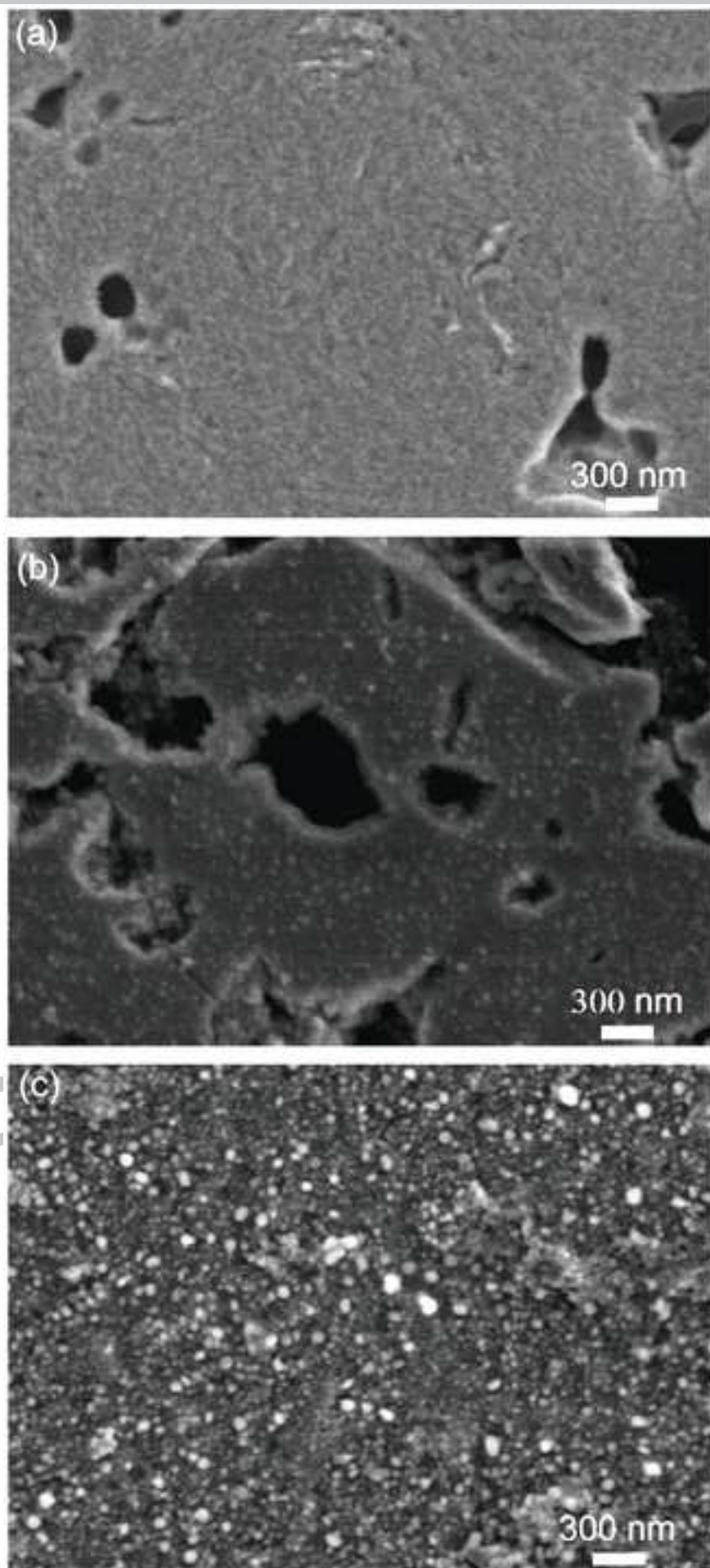
Fig. 5 Variation of microhardness, crystallite size and lattice strain of Fe-14Cr-10Y<sub>2</sub>O<sub>3</sub> powder during processing: (a) as a function of milling time; (b) as a function of annealing temperatures.



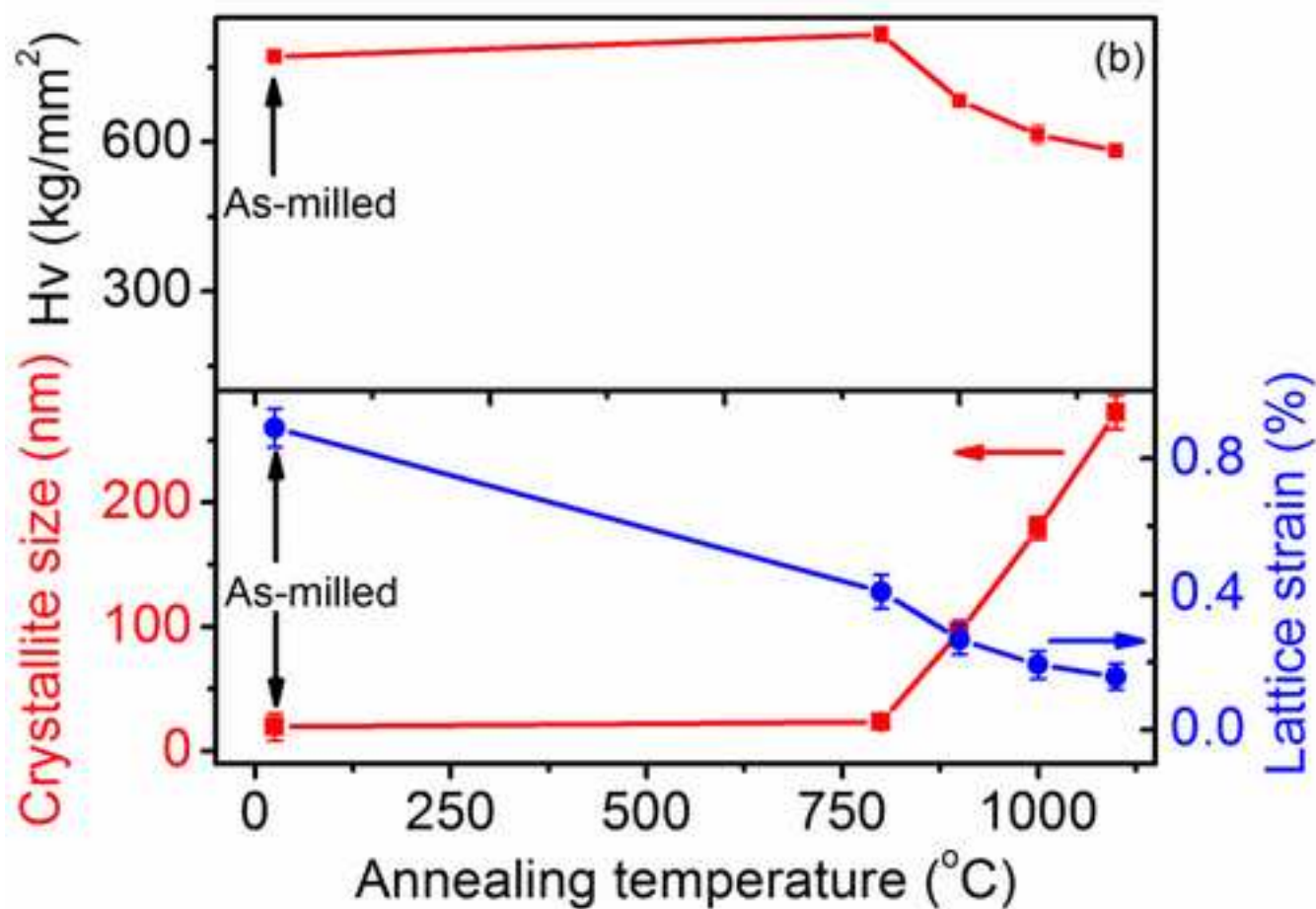
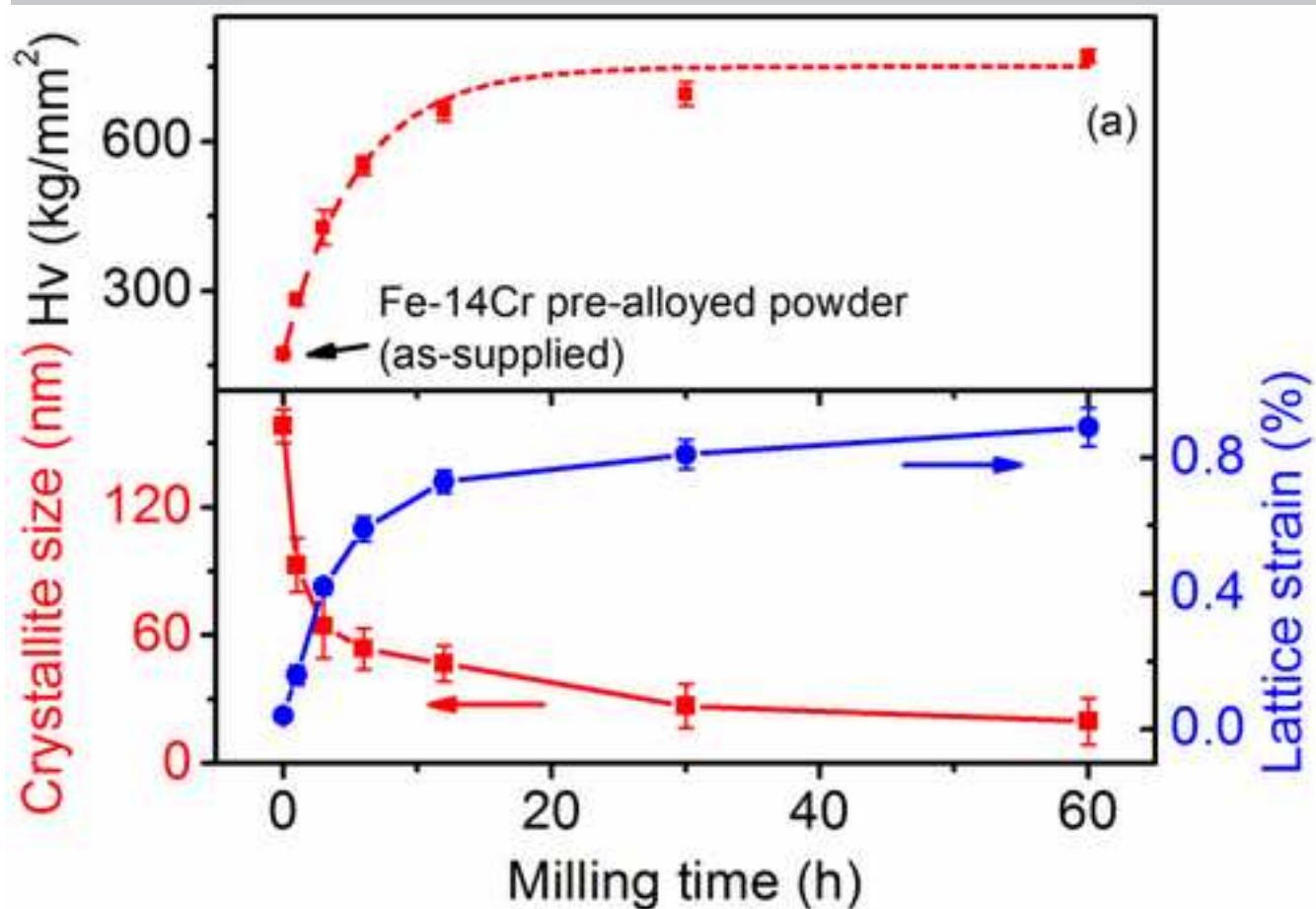












**Highlights**

*In-situ* powder neutron diffraction to study precipitate formation in ODS steel.

First real time observation of nano-precipitate formation during processing.

Y<sub>2</sub>O<sub>3</sub> particles were fully dissolved into steel matrix during mechanical alloy.

The precipitation occurred during annealing of as-milled powder above 900°C.